

# Low dielectric loss ceramics in the $\text{Mg}_4\text{Nb}_2\text{O}_9$ - $\text{ZnAl}_2\text{O}_4$ - $\text{TiO}_2$ ternary system

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## Abstract

This study used a traditional solid-state reaction method to prepare a series of composite ceramics in the  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9$ -( $0.3-x$ ) $\text{ZnAl}_2\text{O}_4$ - $x\text{TiO}_2$  ternary system. Crystalline phases and microstructure of  $\text{Mg}_4\text{Nb}_2\text{O}_9$ - $\text{ZnAl}_2\text{O}_4$ - $\text{TiO}_2$  dielectric ceramic composites were investigated and correlated with the relevant dielectric properties. It was observed that the addition of  $\text{Ti}^{4+}$  substituted  $\text{Nb}^{5+}$  in the  $\text{Mg}_4\text{Nb}_2\text{O}_9$  structure, which promoted the decomposition of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  to form the second phase,  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ , during sintering. The synergistic effect of  $\text{ZnAl}_2\text{O}_4$ - $\text{TiO}_2$  co-doping promoted the  $\text{Mg}_4\text{Nb}_2\text{O}_9$

ceramic densification. The sample  $(0.7\text{Mg}_4\text{Nb}_2\text{O}_9-(0.3-x)\text{ZnAl}_2\text{O}_4-x\text{TiO}_2)$  with  $x = 0.15-0.2$  exhibited dielectric constants of 13-14, larger than those of  $\text{ZnAl}_2\text{O}_4$ ,  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ , due to the  $\text{NbO}_6$  octahedra distortion resulting from the substitution of  $\text{Al}^{3+}/\text{Ti}^{4+}$  for  $\text{Nb}^{5+}$  in  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ . The long-range order of the  $\text{NbO}_6$  octahedra was enhanced by co-doping  $\text{ZnAl}_2\text{O}_4$  and  $\text{TiO}_2$ , thereby enhancing the  $Q_{xf}$  value. A dielectric constant of 13.1,  $Q_{xf}$  value of 366,000 GHz and a  $\tau_f$  of  $-60.8\text{ppm}/^\circ\text{C}$  were obtained from  $1300^\circ\text{C}$  sintered  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9-0.15\text{ZnAl}_2\text{O}_4-0.15\text{TiO}_2$ . These results show that  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9-0.15\text{ZnAl}_2\text{O}_4-0.15\text{TiO}_2$  ceramic is a good candidate for microwave electronic device applications.

Keywords: dielectric loss,  $\text{Mg}_4\text{Nb}_2\text{O}_9$ ,  $\text{ZnAl}_2\text{O}_4$ ,  $\text{TiO}_2$ , microwave ceramics

## 1. Introduction

Low-permittivity dielectric ceramics are used for millimeter-wave communication and as microwave ceramic substrates. As the permittivity decreases, the signal transmission speed increases. Dielectric ceramics with properties of temperature-stability, low-permittivity and a high  $Q_{xf}$  are required in millimeter-wave applications. High  $Q_{xf}$  dielectric ceramics minimize circuit insertion losses and can be used for highly selective filters. Searching for new microwave dielectric ceramics with high-temperature stability, low permittivity, high  $Q_{xf}$  and low cost has always attracted much attention [1-3]. The microwave dielectric properties of ceramics are determined by several

parameters, including the phase composition, the processing conditions and their ultimate densification/porosity [4]. One effective method for obtaining a lower temperature-sintered microwave dielectric ceramic with high  $Q_{xf}$  and near-zero  $\tau_f$  values is by adding low-temperature-fired ceramics to the dielectric [5-6].

Ogawa et al. [7] first reported the microwave dielectric properties ( $\epsilon_r = 12.4$ ,  $Q_{xf} \sim 19,400$  GHz,  $\tau_f = -70$  ppm/ $^{\circ}$ C) of  $Mg_4Nb_2O_9$  ceramics sintered at  $1400^{\circ}$ C for 10 h.  $Mg_4Nb_2O_9$  ceramic exhibits an ordered corundum structure in which the  $NbO_6$  octahedral layer along the c axis is separated by the  $MgO_6$  octahedral layer and the cation vacancy layer. In contrast, the  $NbO_6$  octahedral layer along the b axis is sandwiched by two  $MgO_6$  octahedral layers [8].  $Mg_4Nb_2O_9$  ceramics have gained much attention due to their high  $Q_{xf}$  and low  $\epsilon_r$  value [9-11]. However, the drawbacks of  $Mg_4Nb_2O_9$  ceramics, such as a higher sintering temperature and a significant negative  $\tau_f$ , adversely affect their application. The addition of  $TiO_2$  with positive  $\tau_f$  to  $Mg_4Nb_2O_9$  ceramics has been used to improve the  $\tau_f$  [12].

$ZnAl_2O_4$  ceramic exhibiting a spinel structure has been considered a potential microwave ceramic substrate material [13-15]. Surendran et al. first reported the microwave dielectric properties ( $\epsilon_r = 8.5$ ,  $Q_{xf} \sim 56,300$  GHz,  $\tau_f = -79$  ppm/ $^{\circ}$ C) of  $ZnAl_2O_4$  ceramic [13]. Zheng et al. [14] reported that good dielectric properties ( $\epsilon_r = 8.56$ ,  $Q_{xf} = 106,000$  GHz and  $\tau_f = -63$  ppm/ $^{\circ}$ C) can be obtained for  $1650^{\circ}$ C sintered

ZnAl<sub>2</sub>O<sub>4</sub> ceramic. The Q×f of ZnAl<sub>2</sub>O<sub>4</sub> ceramic sintered at 1600°C was enhanced by forming a (Zn<sub>1-x</sub>Mg<sub>x</sub>)Al<sub>2</sub>O<sub>4</sub> solid solution which reached above 140,000 GHz [15]. The addition of 2 wt% TiO<sub>2</sub> promoted the densification and dielectric properties of Zn<sub>0.9</sub>Mg<sub>0.1</sub>Al<sub>2</sub>O<sub>4</sub> sintered at 1500°C ( $\epsilon_r = 8.57$ , Qxf ~ 180,800 GHz,  $\tau_f = -41.5$  ppm/°C) [16].

Due to crystal structure differences, Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>, ZnAl<sub>2</sub>O<sub>4</sub> and TiO<sub>2</sub> cannot form a solid solution, instead forming ceramic matrix composites with adjustable dielectric properties. The proper addition of ZnAl<sub>2</sub>O<sub>4</sub> and TiO<sub>2</sub> may promote the densification, improve the quality factor and compensate the temperature coefficient ( $\tau_f$ ) of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> ceramics. To our knowledge, there are very few reported investigations into the behaviour of the Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>- ZnAl<sub>2</sub>O<sub>4</sub>-TiO<sub>2</sub> composites which might exhibit promising features for microwave dielectric ceramics. In a previous study, the xMg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-(1-x)/2ZnAl<sub>2</sub>O<sub>4</sub>-(1-x)/2TiO<sub>2</sub> (x = 0.4-0.8) ternary system with quality factors between 10,500 and 120,000 was investigated [17]. This study designed and prepared a series of composite ceramics in the 0.7Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-(0.3-x)ZnAl<sub>2</sub>O<sub>4</sub>-xTiO<sub>2</sub> ternary system via a traditional solid-state reaction method. Crystalline phases and microstructure of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-ZnAl<sub>2</sub>O<sub>4</sub>-TiO<sub>2</sub> dielectric ceramic composites were investigated and correlated with the relevant dielectric properties.

## 2. Experimental procedure

According to the stoichiometric ratio of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{ZnAl}_2\text{O}_4$ , barium niobate and zinc aluminate powders were prepared via the mixed oxides process with reagent-grade  $\text{MgO}$ ,  $\text{Nb}_2\text{O}_5$ ,  $\text{ZnO}$  and  $\text{Al}_2\text{O}_3$ . The calcination conditions of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  powder were held at a temperature of  $1300^\circ\text{C}$  for 3h. The  $\text{ZnAl}_2\text{O}_4$  powder was calcined at  $1200^\circ\text{C}$  for 2h. The  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9\text{-}y\text{ZnAl}_2\text{O}_4\text{-}x\text{TiO}_2$  ternary systems; (MZ015:  $x = 0$ ,  $y=0.15$ ), (MZT015:  $x = 0.15$ ,  $y=0.15$ ), (MZT175:  $x = 0.175$ ,  $y=0.125$ ), (MZT020:  $x = 0.2$ ,  $y=0.1$ ) and (MT015:  $x = 0.15$ ,  $y=0$ ) were prepared from mixtures of reagent-grade  $\text{TiO}_2$ ,  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{ZnAl}_2\text{O}_4$  powders, and the mixed powders were then milled for 3 h using Y-TZP balls. The milled powders were dried in an oven and PVA was then added for granulation. The powders were uniaxially pressed at 255 MPa into disks of 10 mm diameter and 5 mm thickness. These pressed disks were debinded at  $450^\circ\text{C}$  for 1 h and sintered at  $1250^\circ\text{C}$  -  $1500^\circ\text{C}$  for 3 h.

The crystalline phases of sintered pellets were determined by X-ray diffractometry (Bruker, D2 Phaser, Cu-K $\alpha$  radiation, Karlsruhe, Germany). The relative fractions of the constituent phases were quantitatively analyzed from the XRD data using Bruker Topas v4.2 software. The relative densities were calculated from the ratios of apparent density and true density of the sintered disks. Archimedes' method was used to measure the apparent densities of the sintered samples. The sintered disks

were ground into powder and the true densities of the ground powders were measured using helium pycnometry (Quantachrome, ULTRAPYC 1200e, Boynton Beach, FL, USA). Scanning electron microscopy (JEOL JSM-5600F, Tokyo, Japan), transmission electron microscopy (JEOL, JSM-2100F, Tokyo, Japan) and energy dispersive spectroscopy (EDS, Oxford Instruments, 6587, High Wycombe, UK) were used to observe the sintered pellets' microstructure, crystalline phase and chemical composition. For SEM analysis, the surface of the ceramics was ground using SiC 1200 grit paper and polished using diamond paste. The polished samples were then thermally etched at 1200°C for 5 min in air. Thin foils for TEM observation were prepared via the conventional technique: the sintered disks were sliced to a thickness of ~200  $\mu\text{m}$  and then mechanically polished to a thickness of ~30  $\mu\text{m}$  followed by ion-beam thinning to electron transparency. Raman spectra were measured by a Raman spectrometer (Dong Woo 500i, Gyeonggi-do, South Korea) with conditions of a detecting time of 50 s and resolution of 1  $\text{cm}^{-1}$ . Samples were excited by an Ar ion laser beam with a wavelength of 532 nm and power output of 35 mW.

The relative permittivity ( $\epsilon_r$ ) and quality factor (Q) at microwave frequency were measured with the Hakki-Coleman dielectric resonator method using a HP8757D (Agilent Technologies, Palo Alto, CA) network analyzer and a HP8350B (Agilent Technologies) sweep oscillator. The Q value was measured using the TE011 resonant

peak and  $\tau_f$  was obtained by measuring the resonant frequency in the temperature range of 25–85°C. The  $\tau_f$  value (ppm/°C) was calculated by noting the change in resonant frequency.

### 3. Results and discussion

Figure 1 shows the XRD patterns of the MZT015 sintered at various temperatures. All the samples had a well-defined main phase;  $\text{Mg}_4\text{Nb}_2\text{O}_9$ , a minor phase of  $\text{ZnAl}_2\text{O}_4$  and an evident second phase of  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  were observed. The diffraction peak of the  $\text{TiO}_2$  phase was not observed in the XRD profiles. Su et al. [12], who reported that the  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  phase formed after sintering of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  with  $\text{TiO}_2$  as an additive, also observed consistent results. The diffraction angles of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  phases shifted to higher values as the sintering temperature increased. This suggested that the unit cell volumes of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  decreased with increasing sintering temperature [18-19]. Table S1 (supplementary materials) shows the lattice parameters of the MZT015 sintered at various temperatures. The lattice parameters of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  decreased with increasing sintering temperature due to the increase in the ion substitution of  $\text{Ti}^{4+}$  (ionic radius = 0.60 nm) for  $\text{Nb}^{5+}$  (ionic radius = 0.61 nm) [20]. Table S2 (supplementary materials) shows the phase content of the samples sintered at 1300°C. As the  $\text{TiO}_2$  content increased from 15 mol% to 20 mol%, the content of the  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  phase increased from 32.2 wt% to 41.3 wt% in the

0.7Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-(0.3-x)ZnAl<sub>2</sub>O<sub>4</sub>-xTiO<sub>2</sub> ternary system, while the content of the ZnAl<sub>2</sub>O<sub>4</sub> phase remained almost unchanged (at about 5 wt%). The amounts of the Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> phase in MZ015 and MT015 were 12.7 wt% and 45.5 wt%, respectively. The phase diagram of Nb<sub>2</sub>O<sub>5</sub>-MgO predicts that the Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> coexist at equilibrium because the molar ratio of Nb<sub>2</sub>O<sub>5</sub> to MgO is slightly larger than 20/80 [21]. These results suggest that the addition of Ti<sup>4+</sup> dissolved in Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> mainly replaced Nb<sup>5+</sup>, which thus promoted the decomposition of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and formed the second phase of Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> [12].

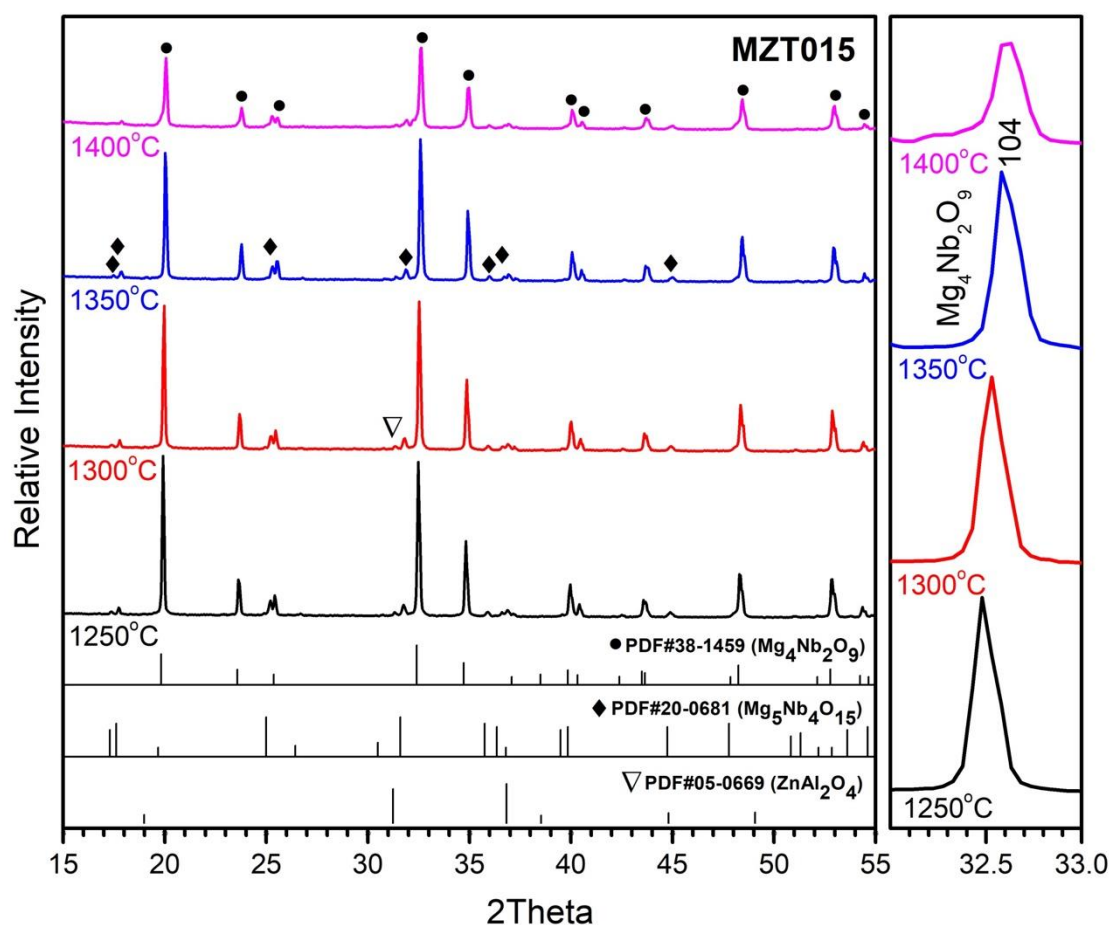




Fig. 1 XRD patterns of the MZT015 dielectric ceramics sintered at various temperatures.

Figure 2 shows the relative densities of the samples sintered at various temperatures. For the MZ015 and MT015 sintered disks, the relative densities were not greater than 90% until the sintering temperature reached 1400°C. The samples in the  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9$ -( $0.3-x$ ) $\text{ZnAl}_2\text{O}_4$ - $x\text{TiO}_2$  ternary system initially had relative densities higher than 95%. These increased slightly with increasing sintering temperature and reached a maximum value in the sintering temperature range from 1300°C to 1350°C. Based on the system of  $\text{Nb}_2\text{O}_5$ - $\text{MgO}$ , the liquidus temperature decreases when increasing the molar ratio of  $\text{Nb}_2\text{O}_5$  to  $\text{MgO}$  in the coexistence region of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  [21]. The addition of  $\text{Ti}^{4+}$  substituting  $\text{Nb}^{5+}$  in the  $\text{Mg}_4\text{Nb}_2\text{O}_9$  structure made the sintered samples become Nb-excess and decreased the liquidus temperature. The addition of  $\text{Ti}^{4+}$  reduced the liquidus temperature, which reduced the activation energy of sintering and high sinterability at a low temperature [22]. Huang et al. [23] developed low-loss microwave dielectrics using  $(\text{Mg}_{1-x}\text{Zn}_x)_4\text{Nb}_2\text{O}_9$  solid solution; they concluded that the addition of  $\text{Zn}^{2+}$  decreased the densification temperature of  $(\text{Mg}_{1-x}\text{Zn}_x)_4\text{Nb}_2\text{O}_9$  dielectric from 1400°C to 1340°C. The synergistic effect of the  $\text{ZnAl}_2\text{O}_4$ - $\text{TiO}_2$  co-doping enhancing the densification of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  ceramics was observed in this study.

At a sintering temperature of 1300°C, the MZT015 sample exhibited the highest relative densities compared with other compositions.

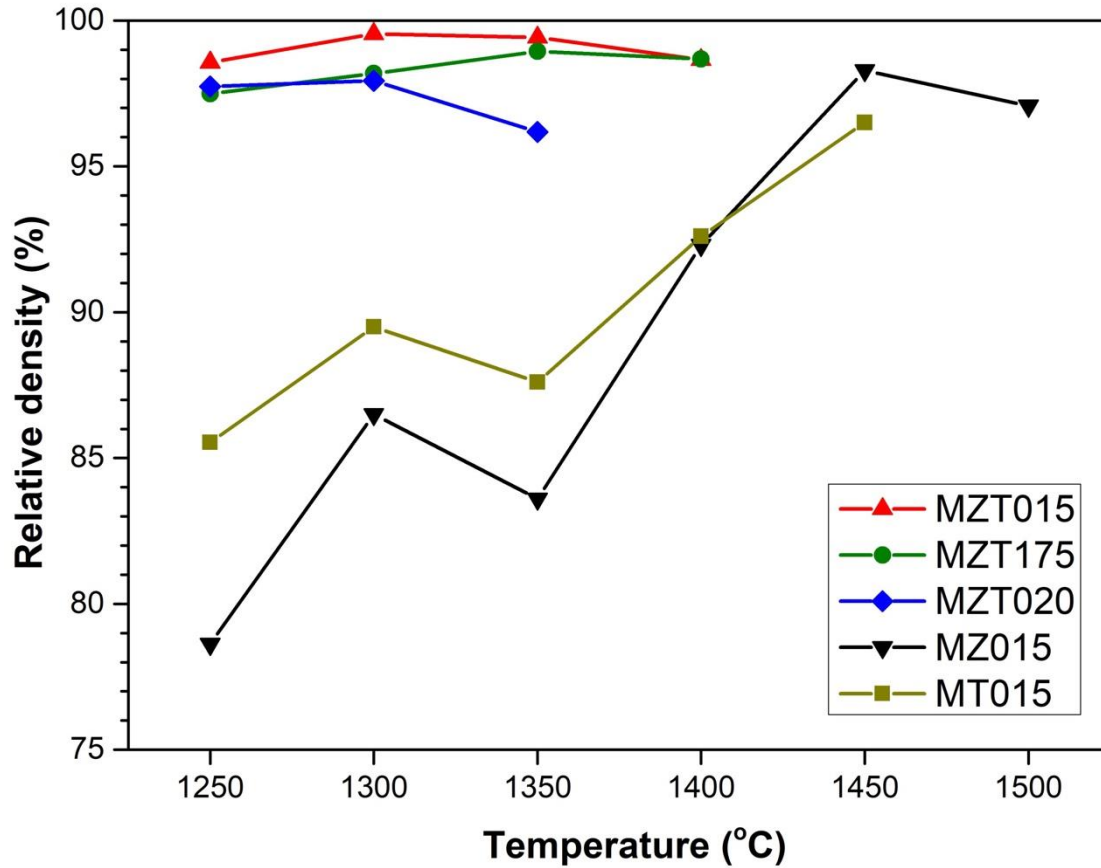


Figure 2 Relative densities of the  $0.7\text{Mg}_4\text{Nb}_2\text{O}_9\text{-yZnAl}_2\text{O}_4\text{-xTiO}_2$  ternary dielectrics sintered at various temperatures.

The SEM micrographics of the MZT015 sintered at various temperatures and MZT175 sintered at 1400°C are shown in Figure 3. All samples exhibited a dense microstructure, which is consistent with the relative sintered density results. The incidence of large and elongated matrix grains was increased by increasing the sintering temperature. The MTZ015 sample sintered at 1250°C for 3 h had a grain size around 5  $\mu\text{m}$ , as shown in Fig 3(a). When the sample was sintered at 1350°C for 3 h, the grains in the sintered

pellet became elongated with dimensions larger than 10  $\mu\text{m}$ , as indicated in Fig 3(c).

The MTZ175 sintered at 1400°C for 3 h had a matrix grain size larger than 15  $\mu\text{m}$ , as shown in Fig 3(d). Precipitates with small grain size located inside the grains as intragranular precipitates, and also at the grain boundaries or triple junctions, were observed. The EDS analysis results obtained from the regions marked A, B and C in Fig. 3(d) are tabulated in Table S3 (supplementary materials). The (Mg+Zn) to (Nb+Al+Ti) molar ratio of large matrix grains was 2.1, corresponding to the composition of  $\text{Mg}_4\text{Nb}_2\text{O}_9$ . The intragranular precipitate, point B in Fig 3(d), had an (Mg+Zn) to (Nb+Al+Ti) molar ratio of 1.18 and was compatible with the composition of  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ . The grain located at the triple junction, as indicated by the arrow in Fig 3(d), had an (Mg+Zn) to (Nb+Al+Ti) molar ratio of 0.56. It had a very low  $\text{Nb}^{5+}$  content, which was considered as a (Mg/Zn) $\text{Al}_2\text{O}_3$  solid solution based on the XRD analysis results (Figure 1). The  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  and  $\text{ZnAl}_2\text{O}_4$  phases existed in the 1300°C sintered MZT015 sample and can also be identified by the HRTEM images, diffraction patterns and the corresponding fast Fourier transform (FFT) patterns (Fig. S1, supplementary materials).

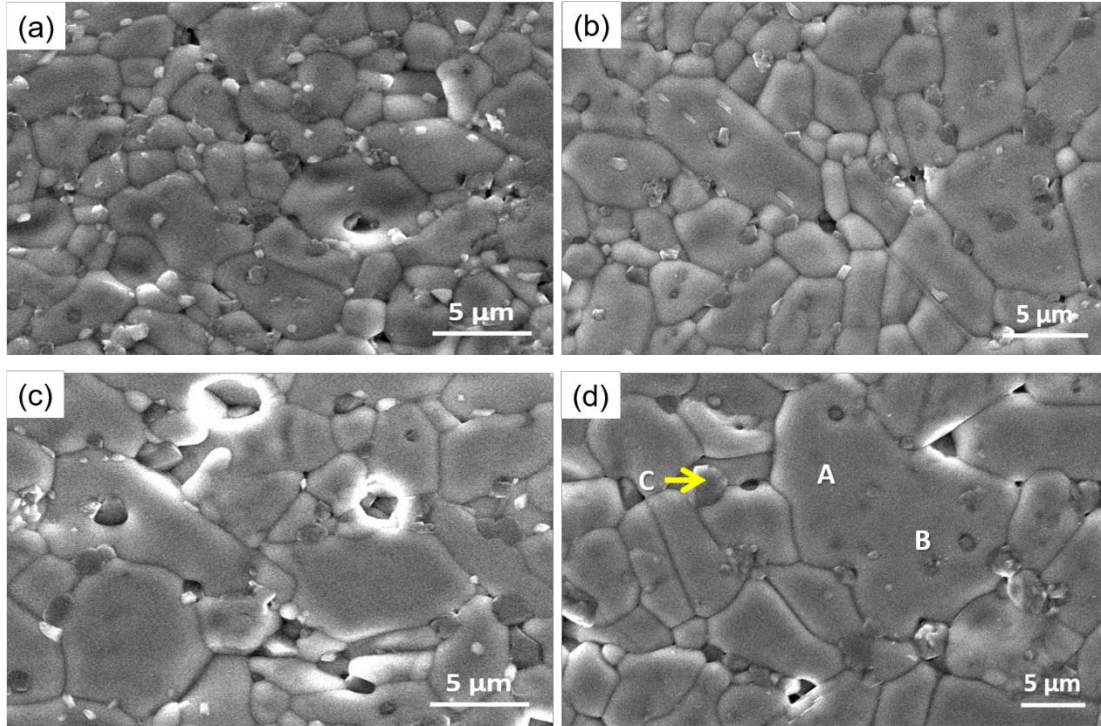


Fig. 3 SEM microstructures of the MZT015 sintered at various temperatures (a)

1250°C, (b) 1300°C, (c) 1350°C, and (d) MZT175 sintered at 1400°C.

The previous paragraph suggests that a large proportion of  $\text{Al}^{3+}$  in the  $\text{ZnAl}_2\text{O}_4$  and  $\text{Ti}^{4+}$  in the  $\text{TiO}_2$  diffused into the  $\text{Mg}_4\text{Nb}_2\text{O}_9$  lattice and a large proportion of  $\text{Mg}^{2+}$  migrated into the  $\text{ZnAl}_2\text{O}_4$  from the  $\text{Mg}_4\text{Nb}_2\text{O}_9$ . As the chemical composition of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  changes from stoichiometric to Nb-rich phase, the single  $\text{Mg}_4\text{Nb}_2\text{O}_9$  phase becomes the mixture phases of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  and  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$  [21]. Bezjak et al. [24] investigated the synthesis and polymorphic phase transition of  $\text{Ba}_4\text{Nb}_2\text{O}_9$  and observed that well-crystallized hexagonal  $\text{Ba}_4\text{Nb}_2\text{O}_9$  grains tended to decompose into BaO-rich amorphous phase and nanocrystalline  $\text{Ba}_5\text{Nb}_4\text{O}_{15}$  during sintering. They inferred that the substitution of  $\text{Al}^{3+}$  and  $\text{Ti}^{4+}$  for  $\text{Nb}^{5+}$  in  $\text{Mg}_4\text{Nb}_2\text{O}_9$  may promote the decomposition of

Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> into Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> and that the MgO-rich amorphous phase easily reacts with ZnAl<sub>2</sub>O<sub>4</sub> and forms (Mg/Zn)Al<sub>2</sub>O<sub>4</sub> solid solution.

The Raman spectra of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and MZT015 sintered samples are displayed in Fig.

4. Strong Raman active modes were observed at 330 cm<sup>-1</sup>, 380 cm<sup>-1</sup>, and 810 cm<sup>-1</sup>, which were assigned to the symmetric bending modes (F<sub>2g</sub> mode) and stretching modes (A<sub>1g</sub> mode) of NbO<sub>6</sub> octahedra with Oh symmetry, respectively [25]. The significant distortion of NbO<sub>6</sub> octahedra resulted in the Raman peak broadening or splitting. At about 810 cm<sup>-1</sup>, A<sub>1g</sub> mode, the strongest band was ascribed to the shortest Nb-O bond length. Sample MZT015 displayed the A<sub>1g</sub> mode split into three Raman-active modes. This was attributed to the presence of different Nb-O bond distances resulting from the coexistence of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>. In addition, a higher wave number of the A<sub>1g</sub> mode in MZT015 (818 cm<sup>-1</sup>) was observed compared with Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> (812 cm<sup>-1</sup>). This was due to the decrease in the oxygen octahedron size [26] resulting from the Ti<sup>4+</sup> substituting Nb<sup>5+</sup>. The F<sub>2g</sub> mode is associated with the internal vibrations of an oxygen octahedron. Figure 4 shows the F<sub>2g</sub> mode split into a doublet at 330 and 380 cm<sup>-1</sup> due to the empty octahedra resulting from a slight local departure from the P $\bar{3}$ c1 space group [27]. This was expected to be split due to the distortion of NbO<sub>6</sub> octahedra for MZT015. Phonons of MZT015 and Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> exhibited nearly the same peak position of the F<sub>2g</sub> mode; this was because the F<sub>2g</sub> mode was not affected by the slight lattice

distortions reported by Siny et al. [28]. The  $F_{2g}$  mode is only sensitive to long-range order on the  $NbO_6$  octahedra, while the  $A_{1g}$  mode is caused by either long-range or short-range order [29]. The narrower band width and higher intensity of the  $F_{2g}$  mode are characteristic of the enhanced level of ordering. MZT015 exhibited higher intensities and a narrower peak width of the  $F_{2g}$  mode than  $Mg_4Nb_2O_9$ , suggesting that long-range order was enhanced for sample MZT015. This may be due to the aliovalent  $Al^{3+}/Ti^{4+}$  cations and  $Nb^{5+}$  that tend to occupy specific  $NbO_6$  octahedron sites to decrease the lattice strain, resulting in an ordered crystal structure [28].

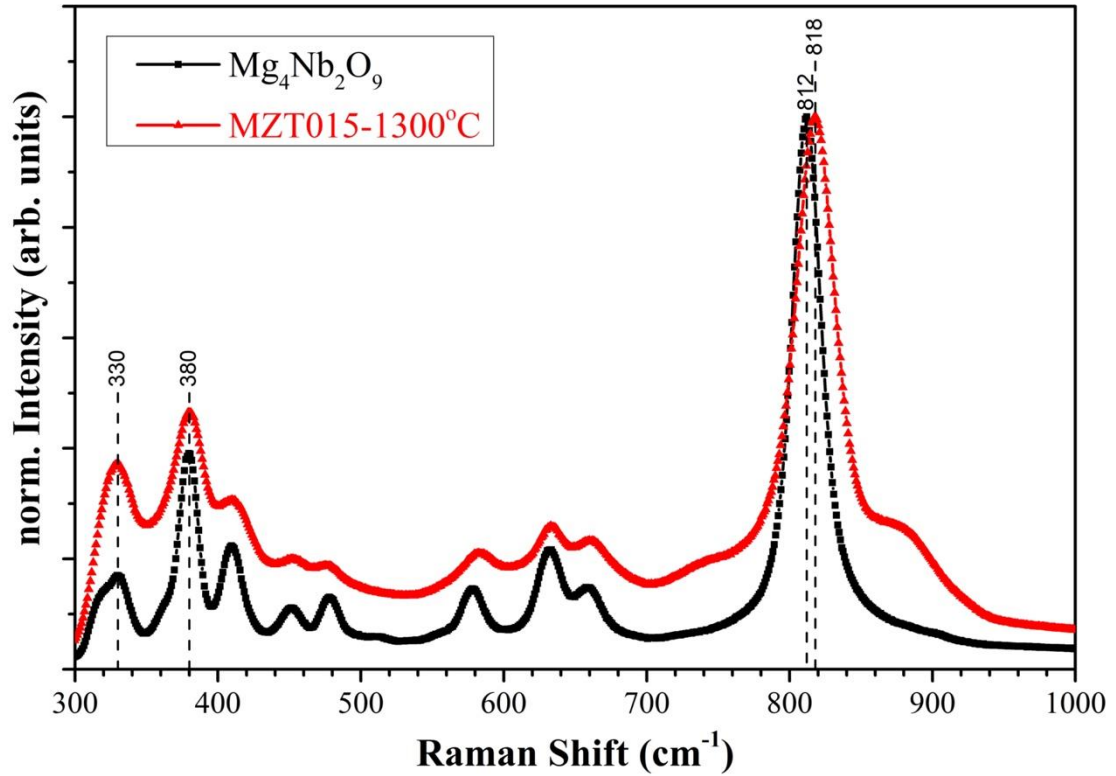


Fig.4 Raman spectra of  $Mg_4Nb_2O_9$  and MZT015 sintered at 1300°C.

Table I shows the variation of the dielectric properties of the samples with different sintering temperatures. The dielectric properties of  $Mg_4Nb_2O_9$ ,  $Mg_5Nb_4O_{15}$ ,  $ZnAl_2O_4$

and TiO<sub>2</sub> reported in the literature are tabulated in Table II. It is well known that the relative density and phase constituent determine the dielectric constant. The dielectric constant of the sample MZ015, without the addition of TiO<sub>2</sub> ( $\epsilon_r = 105$ ), was 12.8, which was the lowest among these samples owing to the highest number of pores ( $\epsilon_r = 1$ ). As listed in Table II, the dielectric constants of Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>, Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>, ZnAl<sub>2</sub>O<sub>4</sub> and MgAl<sub>2</sub>O<sub>4</sub> phases are all lower than 13. The MZT sample (0.7 Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-(0.3-x) ZnAl<sub>2</sub>O<sub>4</sub>-xTiO<sub>2</sub>) with  $x = 0.15-0.2$  and the MT015 samples exhibited dielectric constants between 13 and 14. This is due to the larger NbO<sub>6</sub> octahedra distortion [27] resulting from the substitution of Al<sup>3+</sup>/Ti<sup>4+</sup> for Nb<sup>5+</sup> in Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>, thereby resulting in a higher dielectric constant. The Qxf value is dependent on the relative density, constituent phase and the ordering of cations in NbO<sub>6</sub> octahedra [4]. The Qxf value of the samples increased with increasing sintering temperature and reached a maximum value, then declined, which showed a similar trend to that of the relative density behaviour. The maximum Qxf value for the MZT015, MZT175 and MZT020 samples were 366,000, 296,000 and 176,000, respectively. The maximum Qxf value decreased with the increase of the TiO<sub>2</sub> addition, which was due to the amount of the second phase, Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>, which increased with increasing TiO<sub>2</sub> addition.

Table I Dielectric properties of the samples sintered at different temperatures.

| MZT015 | MZT175 | MZT020 | MT015 | MZ015 |
|--------|--------|--------|-------|-------|
|--------|--------|--------|-------|-------|

### Sintering

| Temperature<br>(°C) | $\epsilon_r$ | Qxf* | $\tau_f^+$ | $\epsilon_r$ | Qxf  | $\epsilon_r$ | Qxf  | $\epsilon_r$ | Qxf   | $\epsilon_r$ | Qxf   |
|---------------------|--------------|------|------------|--------------|------|--------------|------|--------------|-------|--------------|-------|
| <b>1250</b>         | 13.6         | 208k | -          | 13.6         | 230k | 13.8         | 147k | -            | -     | -            | -     |
| <b>1300</b>         | 13.1         | 366k | -60.8      | 13.7         | 296k | 13.6         | 66k  | -            | -     | -            | -     |
| <b>1350</b>         | 13.1         | 325k | -62.3      | 13.5         | 274k | 13.2         | 32k  | -            | -     | -            | -     |
| <b>1400</b>         | 13.2         | 341k | -64.3      | 13.2         | 122k | -            | -    | 13.0         | 16.2k | 12.8         | 13.7k |

\*unit of Qxf: GHz, +unit of  $\tau_f$ : ppm/°C

Table II Dielectric properties of  $\text{Mg}_4\text{Nb}_2\text{O}_9$ ,  $\text{ZnAl}_2\text{O}_4$ ,  $\text{TiO}_2$ ,  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ , and  $\text{MgAl}_2\text{O}_4$  reported in the literature

| Materials                             | $\epsilon_r$ | Qxf(GHz) | $\tau_f$ (ppm/°C) | ref            |
|---------------------------------------|--------------|----------|-------------------|----------------|
| $\text{Mg}_4\text{Nb}_2\text{O}_9$    | 12.4         | 192268   | -70.5             | Yoshida [9]    |
| $\text{ZnAl}_2\text{O}_4$             | 8.5          | 56300    | -79               | Huang [15]     |
| $\text{TiO}_2$                        | 105          | 17600    | 411               | Surendran [13] |
| $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ | 11.3         | 43300    | -58               | Wu [30]        |
| $\text{MgAl}_2\text{O}_4$             | 8.75         | 68900    | -75               | Surendran [31] |

Since the  $\text{Mg}_4\text{Nb}_2\text{O}_9$  phase exhibited a higher Qxf value than the  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ , the presence of the second phase,  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ , degraded the Qxf value of the samples. The MZT015 and MZT175 sintered disks exhibited higher Qxf values than those of the end



members. The ordering of cations in  $\text{NbO}_6$  octahedra has been shown to dominate the  $Q \times f$  value [32]. The substitution of aliovalent  $\text{Al}^{3+}/\text{Ti}^{4+}$  for  $\text{Nb}^{5+}$  enhanced the long-range order of  $\text{NbO}_6$  octahedra for MZT015 and MZT175, which had a significantly beneficial effect on  $Q \times f$  values. Huang et al. [23] reported that the substitution of  $\text{Zn}^{2+}$  for  $\text{Mg}^{2+}$  in  $\text{Mg}_4\text{Nb}_2\text{O}_9$  can also substantially increase the  $Q \times f$  value. Moreover, the  $Q \times f$  value of  $\text{ZnAl}_2\text{O}_4$  ceramic could be significantly improved by forming a  $(\text{Zn}_{1-x}\text{Mg}_x)\text{Al}_2\text{O}_4$  solid solution [15]. Therefore, a low dielectric loss  $\text{Mg}_4\text{Nb}_2\text{O}_9$  ceramic can be obtained by co-doping the proper amount of  $\text{ZnAl}_2\text{O}_4$  and  $\text{TiO}_2$ . The  $\tau_f$  is mainly determined by the relative sintered density and the constituent phase. For MZT015, the  $\tau_f$  was about -60 ppm/ $^{\circ}\text{C}$  and almost independent of the sintering temperature due to there being no significant constituent phase change. It is difficult to adjust the  $\tau_f$  to zero due to the chemical reaction between  $\text{TiO}_2$  and  $\text{Mg}_4\text{Nb}_2\text{O}_9$  during sintering.

#### 4. Conclusions

The development of crystalline phases and microstructures of  $\text{Mg}_4\text{Nb}_2\text{O}_9$ - $\text{ZnAl}_2\text{O}_4$ - $\text{TiO}_2$  dielectric ceramics with different phase compositions after sintering has been investigated. The substitution of  $\text{Al}^{3+}$  and  $\text{Ti}^{4+}$  for  $\text{Nb}^{5+}$  in  $\text{Mg}_4\text{Nb}_2\text{O}_9$  may promote the decomposition of  $\text{Mg}_4\text{Nb}_2\text{O}_9$  into  $\text{Mg}_5\text{Nb}_4\text{O}_{15}$ . The addition of  $\text{Ti}^{4+}$  dissolved in  $\text{Mg}_4\text{Nb}_2\text{O}_9$  mainly substituted  $\text{Nb}^{5+}$ , which led to the chemical composition becoming Nb-excess. This in turn resulted in a decrease in the liquidus temperature and promotion

of the densification. The long-range order on the NbO<sub>6</sub> octahedra was enhanced by the co-doping of ZnAl<sub>2</sub>O<sub>4</sub> and TiO<sub>2</sub> to Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>, thereby increasing the Q×f value. The sample (0.7Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-(0.3-x)ZnAl<sub>2</sub>O<sub>4</sub>-xTiO<sub>2</sub>) with x = 0.15-0.2 exhibited a dielectric constant of 13-14, larger than ZnAl<sub>2</sub>O<sub>4</sub>, Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>. This was due to the larger NbO<sub>6</sub> octahedra distortion resulting from the substitution of Al<sup>3+</sup>/Ti<sup>4+</sup> for Nb<sup>5+</sup> in Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub> and Mg<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub>. A dielectric constant of 13.1, a high Qxf value of 366,000 GHz and a  $\tau_f$  of -60.8ppm/°C can be obtained for 0.7Mg<sub>4</sub>Nb<sub>2</sub>O<sub>9</sub>-0.15ZnAl<sub>2</sub>O<sub>4</sub>-0.15TiO<sub>2</sub> sintered at 1300°C.

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