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## Characterization of Hard Piezoelectric Lead-Free Ceramics

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#### Abstract

 $K_4CuNb_8O_{23}$  doped  $K_{0.45}Na_{0.55}NbO_3$  (KNN-KCN) ferroelectric ceramics were found to exhibit asymmetrical polarization hysteresis loops, related to the development of an internal bias field. The internal bias field is believed to be the result of defect dipoles of acceptor ions and oxygen vacancies, which lead to piezoelectric "hardening" effect, by stabilizing and pinning of the domain wall motion. The dielectric loss for the hard lead-free piezoelectric ceramic was found to be 0.6%, with mechanical quality factors Q on the order of >1500. Furthermore, the piezoelectric properties were found to decrease and the coercive field increased, when compared with the undoped material, exhibiting a typical characteristic of "hard" behavior. The temperature usage range was limited by the polymorphic phase transition temperature, being 188°C. The full set of material constants was determined for the KNN-KCN materials. Compared with conventional hard PZT ceramics, the leadfree possessed lower dielectric and piezoelectric properties; however, comparable values of mechanical Q, dielectric loss, and coercive fields were obtained, making acceptor modified KNN based lead-free piezoelectric material promising for high-power applications, where lead-free materials are desirable.

#### I. Introduction

Ferroelectric ceramics for high-power applications, such as ultrasonic motors, transformers, and high intensity focused ultrasound (HIFU), demand piezoelectrics with high mechanical quality factors (low mechanical loss) and low dielectric loss to deliver high acoustic power without excessive heat generation and/or thermal runaway. In general, to achieve the "hardening" effect, these materials are acceptor doped, e.g., with Fe<sup>3+,2+</sup>, Mn<sup>3+,2+</sup> substitution onto Zr<sup>4+</sup>/Ti<sup>4+</sup> sites, resulting in the development of acceptor-oxygen vacancy defect dipoles. These dipoles align parallel to the polarization direction, leading to an internal bias, as evident in a horizontal offset in the polarization-electric field (P-E) behavior. This offset effectively increases the coercive field ( $E_C$ ) and reduces or clamps domain wall motion/mobility [1]–[6].

Hard PZT ferroelectric materials, including PZT4 and PZT8 (DOD type I and III) [7], have been the mainstay for high-power applications. However, because of the toxicity of lead oxide in PZT ceramics, it is desirable to develop lead-free piezoelectric ceramics with comparable performance to replace lead-based materials. Recently, high  $d_{33}$  (~300 pC/N) piezoelectrics were reported to be achieved from alkaline niobate-based perovskite materials in the  $K_xNa_{1-x}NbO_3$  (KNN) family [8]–[18], which exhibit "soft" behavior with high dielectric loss, related to the orthorhombic to tetragonal polymorphic phase transition (PPT) compositionally engineered to near room temperature [13]–[15]. In addition to these "soft" KNN-based materials, many researchers have been focusing on "hard" characteristics of KNN based materials, modified by  $K_{5.4}Cu_{1.3}Ta_{10}O_{29}$ ,  $K_4CuNb_8O_{23}$ , or CuO [19]–[23], with piezoelectric coefficients  $d_{33}$  on the order of <100 pC/N and mechanical quality factors Q ~1000. To further study the theoretical and practical applications of hard lead-free piezoelectric materials, it is desirable to have a full set of material constants, including elastic constants, electromechanical coupling factors, piezoelectric coefficients, and dielectric permittivity, and also understand the temperature-dependent piezoelectric behavior.

In this work, high field ferroelectric behavior and temperature dependence of the dielectric and piezoelectric properties were investigated for hard lead-free ceramics, with the full set of material constants determined according to the IEEE piezoelectric standard [24], [25]. The properties were compared with commercial hard PZT4 and PZT8 ceramics.

#### II. Experimental

K<sub>4</sub>CuNb<sub>8</sub>O<sub>23</sub> (KCN) (0.5 mol%) acceptor modified orthorhombic K<sub>0.45</sub>Na<sub>0.55</sub>NbO<sub>3</sub> (KNN) was selected in this study. Raw materials were weighed according to the nominal compositions, vibration milled in anhydrous ethanol for 24 h, dried, and subsequently calcined at 850°C for 2 h. The acceptor dopant KCN was mixed into the calcined powder, subsequently granulated and pressed into pellets and sintered at 1100 to 1160°C for 2 h. The phase purity was examined by x-ray powder diffraction performed on ground sintered ceramics. The density of the pellets was found to be 4.4 g/cm<sup>3</sup> by the Archimedes method for KCN modified KNN, more than 95% of the theoretical. The ceramic disks were polished with a diameter and thickness ratio greater than 20. Fire-on silver paste was applied on the samples as the electrode. The samples were poled at 60 kV/cm and room temperature for 5 min and aged for 24 h before the measurements. The full set of material constants were determined according to the IEEE standard [24] by the resonance and antiresonance frequencies, which were measured using an HP4194A impedance/gain-phase analyzer (Agilent, Santa Clara, CA). The dielectric permittivity and dielectric loss were determined using a multifrequency LCR meter (HP4284A Agilent, Santa Clara, CA) as a function of temperature in a temperature-controlled furnace. High field measurements including polarization hysteresis (P-E) and strain-electric field curves (x-E) were measured at 1 Hz frequency and 40 kV/cm electric fields using a modified Sawyer-Tower circuit and linear variable differential transducer (LVDT), driven by a lock-in amplifier (Model SR 830, Stanford Research Systems, Sunnyvale, CA). The temperature dependence of electromechanical coupling factors were performed on disk samples using an impedance analyzer connected to a high temperature furnace.

#### **III. Results and Discussion**

#### A. Ferroelectric Properties under High Electric Field

Fig. 1 gives the polarization hysteresis (P-E), measured at a field of 40 kV/cm and frequency of 1 Hz for aged (~one day) KNN-KCN and compared to conventional hard PZT, showing asymmetric loops. This horizontal off-set of the P-E loops is the result of building up of the internal bias field  $E_i$  and believed to play an important role in the properties of ceramics [2]– [5]. The mechanisms responsible for the occurrence of an internal bias in the lead-free ferroelectrics are based on the stabilization of domain wall movement. In KCN-modified KNN material, the Cu<sup>2+</sup> acceptor ions are incorporated into the Nb<sup>5+</sup> site, due to their similar ionic radius. Thus, oxygen vacancies are introduced due to valence compensation. The acceptoroxygen vacancy defect dipoles can occupy energetically preferred sites in the lattice and then form anisotropic centers locally or within a domain, preferentially align themselves along the spontaneous polarization, or diffuse into the high-stressed areas of domain walls, experimentally revealed as an internal bias field, stabilizing the polarization, pinning, and/or clamping the domain wall motion [2]. Furthermore, it is reported that KCN/CuO additives in KNN materials also act as a sintering aid, which will generate a liquid phase at the sintering temperature, leading to a grain boundary phase and subsequent build-up of space charge at the grain boundaries. The resulting space charge field is equivalent to an internal bias field that impresses an overall preferred direction of polarization on each crystallite, locking in the ferroelectric domains, as also reported in hard PZT [2].

Fig. 2 presents the unipolar strain as a function of the electric field (x-E) for the lead-free KNN-KCN and compares it to hard PZTs. The strain hysteresis, which is related to the piezoelectric loss, can be obtained from the ratio of the widest part of the x-E loop over the maximum strain level. The hysteresis levels are found to be lower than 10% for all the hard ceramics, due to the pinning/clamping of ferroelastic non-180° domain wall motion.

#### B. Characteristic Properties of Lead-Free Materials Compared with Hard PZT

Table I lists the characteristic properties of hard lead-free KNN-KCN, compared to undoped KNN material and commercial hard PZTs. Compared to undoped KNN material, the KNN-KCN is found to possess lower dielectric permittivities and piezoelectric coefficients, while exhibiting increased mechanical quality factors and lower dielectric loss, indicative of a "hardening" effect. Meanwhile, the coercive fields are found to increase and the remnant polarization decrease and hence the degree of "switchable" polarization is significantly reduced due to domain wall pinning. Of particular interest is the level of the internal bias field for KNN-KCN, while no internal bias is observed for the undoped samples, demonstrating that the acceptor-oxygen vacancy defect dipoles give rise to an internal bias, which leads to domain wall stabilization and thus the "hardening" effect. Compared to conventional hard PZT ceramics, the internal bias field level is found to be on the order of 5 kV/cm, between that of the hard PZT4 (~3 kV/cm) and very hard PZT8 (~7 kV/cm), with higher mechanical quality factors (Q ~1500). The acoustic velocity of KNN based material is found to be higher than PZTs, while the acoustic impedance is decreased, owing to the low density of lead-free materials.

#### C. Dielectric Properties as Function of Temperature

Fig. 3 shows the dielectric permittivity as a function of temperature for KNN-KCN, as compared with a PZT8. The dielectric permittivity is found to be 290 at room temperature for KNN-KCN ceramic, with the Curie temperature on the order of 410°C, higher than the Curie temperature of the PZT. However, a dielectric anomaly exists in KNN-KCN before its Curie temperature, located at a temperature of 188°C, believed to be related to the orthorhombic to tetragonal polymorphic phase transition. The small insert of Fig. 1 shows the dielectric loss as a function of temperature, where the dielectric loss is found to be 0.6% at room temperature, while the dielectric loss increases drastically above the Curie temperature, due to the ionic conduction at elevated temperatures.

#### D. Piezoelectric Properties as a Function of Temperature

The maximum operating temperature for smart structures is generally limited by piezoelectric materials, so piezoelectric materials with broad temperature usage range are desirable. Generally speaking, the usage temperature range of ferroelectric ceramics is limited to less than half of their respective Curie temperatures due to the reduction of the piezoelectric activity, caused by aging effects [26]. For KNN-based ceramic, it is reported that an orthorhombic to tetragonal polymorphic phase transition exists before its Curie temperature, above which the property is found to be greatly deteriorated [9]. Fig. 4 shows the planar electromechanical coupling factor variation as a function of temperature for KNN-KCN ceramics and compares to hard PZTs. It is found that the planar electromechanical coupling  $k_p$  increases till 180°C, above which the properties sharply decrease for KNN-KCN material, related to the orthorhombic to tetragonal phase transformation, while for hard PZT4 and PZT8 ceramics, the properties are found to decrease gradually. Of particular interest is the property degradation observed for PZT-based ceramic in the thermal cycle experiments; however, no degradations occur for KNN-KCN before the  $T_{O-T}$ .

#### IV. Summary

In summary, acceptor-modified KNN lead-free piezoelectrics are prepared by conventional solid-state reaction and characterized. The full set of material constants of lead-free materials, including elastic constants, piezoelectric coefficients, electromechanical coupling factors, and dielectric permittivity, are determined and listed in Tables II, III, and IV and compared with the values of "hard" PZT ceramics. The elastic compliance constants of KNN-KCN are found to be lower than the values of PZT-based hard ceramics, with higher elastic stiffness constants. The piezoelectric strain coefficients  $d_{ij}$  and piezoelectric stress coefficients  $e_{ij}$  are found to be decreased when compared with the hard PZT materials, while the piezoelectric voltage coefficients  $g_{ij}$  and piezoelectric stiffness coefficients  $h_{ij}$  are increased, due to its low dielectric permittivity, being on the order of ~290.

For KNN-KCN, dense samples are obtained since KCN/CuO acts as a sintering aid in KNN material; meanwhile, the valence of the acceptor ions are assumed to be 2+ and substitute onto

the Nb<sup>5+</sup> site due to the similar ion radius, generating  $Cu_{Nb}^{'''} - V_{\partial}$  dipole defects, leading to the development of an internal bias field of ~5 kV/cm, clamping the domain wall movement, playing a "hardening" effect, with associated characteristics of a "hard" effect: Q ~1500, loss ~0.6%, and  $E_C$  ~12 kV/cm. The  $T_C$  and  $T_{O-T}$  are found to be slightly shifted downward when compared with the pure KNN, being on the order of 410 and 188°C, with stable dielectric and piezoelectric behaviors before  $T_{O-T}$ . The temperature usage range of KNN-based ceramics is limited by  $T_{O-T}$ , unlike PZT, which is limited to resistivity and aging effects, usually  $1/2T_C$ . Compared with conventional "hard" PZTs, the KNN-KCN materials possesses lower dielectric and piezoelectric properties; however, they exhibit improved "hard" characteristics, higher acoustic velocity, and lower acoustic impedance, demonstrating that acceptor-doped lead-free ferroelectrics are promising candidates to replace PZT-based hard materials in high-power applications.

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### **Biographies**





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#### Fig. 1.

Polarization hysteresis for hard lead-free KNN-KCN, compared with commercial PZT, showing the internal bias field on the order of 5 kV/cm.









Dielectric permittivity as a function of temperature for hard lead-free KNN-KCN, compared with commercial hard PZT8 (small insert shows the dielectric loss behavior).





Variation of the planar electromechanical coupling factor as a function of temperature for hard lead-free KNN-KCN and compared with commercial PZT.

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Characteristic Properties of KNN-Lead-Free Piezoelectric Ceramics, Compared with Commercial, Hard PZTs.

	°C) $\varepsilon_{33}^{\epsilon}/\varepsilon_{0}$	loss	$P_r(\mathrm{C/m^2})$	$E_C(\mathrm{kV/cm})$	$E_i  ({\rm kV/cm})$	d <sub>33</sub> (pC/N)	k <sub>33</sub>	$\tilde{o}$	$\rho(\mathrm{g/cm}^3)$	$v_3^D$ (m/s)	Z (MRayl)
-KCN 410 188	292	0.6%	0.21	11.6	5	60	0.55	1500	4.4	6250	27.5
(HP) <sup>14</sup> 420 195	496	1.5%	0.33	5.0	Ι	127	0.61	240	4.4	6930	30.5
- 328	1300	0.4%	0.36	14.2	3	289	0.70	500	7.6	4570	34.7
300 —	1000	0.4%	0.27	19.0	7	225	0.64	1000	7.6	4600	35.0

and Compared with Hard PZTs.
KNN-KCN Cerami
$n^2$ ) Constants for H
ess $c_{ij}$ (10 <sup>10</sup> N/ <sub>1</sub>
) and Elastic Stiffn
$s_{ij}$ (10 <sup>-12</sup> m <sup>2</sup> /N
Elastic Compliance

Material	$^{s}_{11}^{E}$	$^{s}_{12}$	$s_{13}^E$	$s_{33}^E$	$^{s}_{44}^{E}$	$s_{66}^E$	${}^{S}_{11}$	$^{s}_{12}^{D}$	${}^{s}_{13}$	$S_{33}^{D}$	<i>u</i> <sup>2</sup> 44	${}^{S}_{66}$
KNN-KCN	8.6	-2.6	-2.1	9.3	22.0	22.3	8.2	-3.0	-1.0	6.4	17.5	22.3
PZT4	12.3	-4.1	-5.2	15.5	39.0	32.7	10.9	-5.4	-2.1	7.9	19.3	32.7
PZT8	11.5	-3.4	-4.8	13.5	31.9	29.8	10.4	-4.4	-2.3	8.0	22.6	29.8
Material	$c_{11}^E$	$c_{12}^E$	$c_{13}^E$	$c_{33}^E$	$c_{44}^E$	$c_{66}^E$	$c_{11}^D$	$c_{12}^D$	$c_{13}^D$	$c_{33}^D$	$c_{44}^D$	$c^D_{66}$
KNN-KCN	14.6	5.6	4.7	12.9	4.6	4.5	14.8	5.9	3.6	17.2	5.7	4.5
PZT4	13.9	7.6	7.1	11.5	2.6	3.1	14.5	8.0	5.7	15.9	5.2	3.1
PZT8	13.7	7.2	7.5	12.3	3.1	3.4	14.0	7.5	6.4	16.1	4.4	3.4

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# Table III

Piezoelectric Coefficients,  $d_{ij}$  (pC/N),  $e_{ij}$  (C/m<sup>2</sup>),  $g_{ij}$  (10<sup>-3</sup> Vm/N),  $h_{ij}$  (10<sup>8</sup> V/m),  $d_h$  (pC/N), Electromechanical Coupling Factors  $k_{ij}$  of KNN-KCN, Compared with Hard PZT.

Material	d <sub>33</sub>	$d_{31}$	$d_{15}$	¢33	$e_{31}$	e 15
KNN-KCN	90	-32	125	8.4	-2.2	5.7
PZT4	289	-126	496	15.1	-5.2	12.7
PZT8	225	-97	330	13.2	-4.0	10.4
Material	833	831	815	$h_{33}$	$h_{31}$	$h_{15}$
KNN-KCN	34.9	-12.3	35.7	50.1	-13.2	20.7
PZT4	25.1	-10.7	38.0	26.9	-9.3	19.7
PZT8	25.4	-10.9	29.0	25.7	-7.8	13.1
Material	$k_{33}$	$k_{31}$	$k_{15}$	$k_{t}$	$k_p$	$d_h$
KNN-KCN	0.55	0.21	0.45	0.50	0.36	26
PZT4	0.70	0.33	0.71	0.51	0.58	37
PZT8	0.64	0.30	0.55	0.48	0.51	31

# Table IV

Dielectric Permittivity,  $\varepsilon_{ij}$  ( $\varepsilon_0$ ), and Dielectric Impermeability Constants,  $\beta$  (10<sup>-4</sup>/ $\varepsilon_0$ ), for KNN-KCN and Compared with Hard PZT.

Material	$^{e}_{33}$	$^{E}_{11}$	<sup>5</sup> 33	$^{e}_{11}$	$\beta_{33}^{T}$	$\beta_{11}^{T}$	$\beta_{33}^S$	$\beta_{11}^S$
KNN-KCN	292	395	190	310	34.2	25.3	52.6	32.3
PZT4	1300	1475	635	730	T.T	6.8	15.8	13.7
PZT8	1000	1290	580	006	10.0	7.8	17.2	11.1