# Electrical stimulation systems for cardiac tissue engineering

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We describe a protocol for tissue engineering of synchronously contractile cardiac constructs by culturing cardiac cells with the application of pulsatile electrical fields designed to mimic those present in the native heart. Tissue culture is conducted in a customized chamber built to allow for cultivation of (i) engineered three-dimensional (3D) cardiac tissue constructs, (ii) cell monolayers on flat substrates or (iii) cells on patterned substrates. This also allows for analysis of the individual and interactive effects of pulsatile electrical field stimulation and substrate topography on cell differentiation and assembly. The protocol is designed to allow for delivery of predictable electrical field stimuli to cells, monitoring environmental parameters, and assessment of cell and tissue responses. The duration of the protocol is 5 d for two-dimensional cultures and 10 d for 3D cultures.

#### INTRODUCTION

The overarching goal of cardiac tissue engineering is to create *in vitro* functional cardiac tissue that can be used as a biological model for studies of cardiac tissue development and/or disease processes, and eventually as an implant to repair injured myocardium. Successfully engineered 3D cardiac tissue should therefore exhibit the important properties of native cardiac tissue, including the assembly of differentiated cardiac cell populations into a 3D syncytium, as well as contractile and electrophysiological functionality.

Although heart tissue was first cultured almost 100 years ago<sup>1</sup>, the maintenance of differentiated cardiac cells *in vitro* using traditional cell culture methods continues to be an issue<sup>2</sup>, as adult cardiomyocytes quickly dedifferentiate *in vitro*<sup>3,4</sup> and neonatal cells are still immature. These facts have driven the development of the biomimetic paradigm of cardiac tissue engineering, which involves the application of physiologically relevant chemical and physical stimuli to cultured cells. A biomimetic approach to cardiac tissue engineering may be designed to recapitulate any number of aspects of the actual *in vivo* environment, including the convection of blood through perfusion<sup>2,5</sup>, the presence of hemoglobin via oxygen carriers in the culture medium<sup>6</sup> and the exposure of cells to a cyclic stretch<sup>7</sup> or to electrical field stimulation<sup>8,9</sup>.

In recent studies in our group, a biomimetic system designed to deliver electrical signals mimicking those in native heart tissue resulted in the progressive development of conductive and contractile properties characteristic of cardiac tissue, including cell alignment and coupling, increased amplitude of synchronous construct contractions and a remarkable level of ultrastructural organization<sup>8,10</sup>. One important area of research is the optimization of the parameters of the applied electrical field stimulus, and so our group has expanded our focus to include studies of the effects of electrical field stimulation on cardiac cell populations. Furthermore, with the growing body of research indicating the importance of cell alignment, we have become interested in studying the

interactive effects of substrate topography and electrical field stimulation in cell monolayers.

The heart is the body's largest bioelectrical source<sup>11</sup>. Many groups have been studying electrical signals in the heart, in the context of arrhythmia, defibrillation, pacing and cardiac development. In terms of electrical simulation of cultured cardiac cells, others have developed *in vitro* models of arrhythmia<sup>12</sup>, mechanoelectrical feedback<sup>13</sup> and protocols for a stable cardiac phenotype in culture<sup>14,15</sup>. In addition, cardiac cells have been 'electrically' stimulated through the modulation of ion channel expression to study electrical signals in cardiac development<sup>16</sup> and cardiac excitability<sup>17,18</sup>. Our group has pioneered the application of electrical signals in cardiac tissue engineering, to enhance functional coupling of the cells and the formation of synchronously contractile tissue constructs<sup>8</sup>.

A bioreactor system with electrical stimulation may, in principle, reproduce any specific electrical stimulus in the physiological range. For cardiac tissue engineering, the signals of interest are those found both in the developing and in the adult heart. The presence of endogenous electrical fields and currents in the developing vertebrate embryo has been widely documented<sup>19</sup>. The main types of electrical currents in embryonic heart are the direct current (DC) signals thought to direct cell migration during the development of the cardiac primitive streak and left-right asymmetry, and the pulsatile signals implicated in the development of the cardiac syncytium<sup>16,19,20</sup>. The protocol presented here allows for the application of pulsatile electrical field stimuli mimicking those in the adult native heart to cells or tissues. A customized chamber (see Fig. 1) is built to allow for (i) the culture of engineered 3D cardiac tissue, (ii) the inclusion of an unpatterned insert to apply pulsatile electrical field stimulation to cell monolayers or (iii) the inclusion of a microabraded patterned insert to study the interactive effects of pulsatile electrical field stimulation and topography on cell alignment and differentiation.

**Figure 1** | Experimental setup for applying pulsatile electrical field stimuli to cardiac cells. (a) Overview of experimental setup. An electrical stimulator generates the pulses, which are transmitted to bioreactors located inside an incubator maintained at 37 °C. (b) Schematic diagram of the electrical stimulation chamber (modified Petri dish with carbon rod electrodes). Either an unabraded monolayer culture insert, a microabraded monolayer culture insert or 3D scaffolds may be placed in between the electrodes. (c) Close-up view of platinum wire threaded through carbon rod electrode. (d) Close-up view of silicone adhesive covering the connection between the platinum wire and electrode (platinum wire comes out of adhesive on the right). (e) Photograph of an assembled electrical stimulation chamber. (f) Close-up view of scaffold positioned between electrodes. (g) Close-up view of abraded monolayer culture insert placed between electrodes.

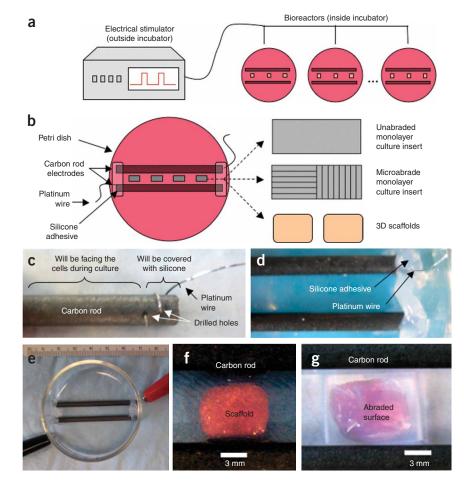
The protocol we present here is for electrical field stimulation of monolayers and tissues in the cardiac tissue engineering context (i.e., to enhance functional performance of cardiac tissues as well as to study the effects of applied electrical fields on cell morphology and differentiation). Given the ubiquity of cellular electrical phenomena, these procedures will likely prove useful in a variety of applications involving electrical field stimulation of cells. In fact, even within our own group, although the procedures we

describe have been extensively used in studies of rat neonatal cardiomyocytes<sup>8,10,21,22</sup>, we have also used subsets of these procedures with C2C12 cells<sup>23</sup>, adipose-derived human mesenchymal stem cells and human embryonic stem cells to study cardiac differentiation, as well as bovine chondrocytes<sup>24</sup> to study cell migration implicated in wound healing. Although we have used many types of cell sources, however, we have not at this point developed advanced methods for measurement of bioelectrical currents<sup>25</sup>, or *in vivo* stimulation<sup>26</sup> of these alternative cell types, and we refer the reader to other published sources.

#### **Experimental design**

The general flow diagram of the complete protocol involving four related processes is shown in **Figure 2**. The culture chamber (Steps 1–9) can be prepared ahead of time and stored for future use, and cells (isolated according to Steps 29–58 of our accompanying cardiac tissue engineering paper<sup>27</sup>) are prepared for monolayer (unpatterned or patterned) (Step 10A) or 3D culture (Step 10B). Next, the culture chamber is assembled, cell culture is established and the electrical stimulation is applied (Steps 11–20). Finally, assessments are performed on either live cells or after fixation (Step 21).

**Culture chamber.** It is desirable to maintain a constant position of the scaffolds with respect to direction of the electrical field gradient, although at the same time not restricting the contractions of cells nor the ability to observe the constructs with a microscope. We



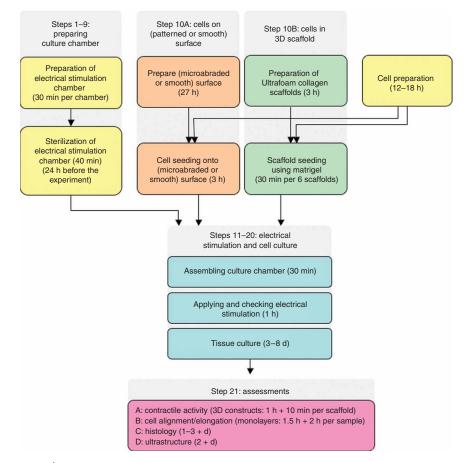
accomplish this task by assembling a culture chamber composed of carbon rod electrodes placed lengthwise along the bottom of a Petri dish and held in place by silicone adhesive (**Fig. 1**). The spacing between the electrodes accommodates the width of the constructs between them. The wires dangle free so as to facilitate making detachable electrical connections, which is necessary to change medium and monitor the cells in culture, and they must be composed of a highly biocompatible material. We choose platinum wire, which is highly compatible, durable and flexible.

All of the components in this system are easily obtainable and (with the exception of the platinum wires) relatively inexpensive. In addition, most of the components are reusable (with the exception of the silicone adhesive and the carbon  $rods^{28}$ ).

**Monolayer versus 3D culture.** Systems for studying biological electrical phenomena may be constructed to examine processes at a variety of hierarchical levels: molecular, cellular, cell population (monolayer) and 3D tissue. Monolayer cultures have the advantages that they require fewer cells, facilitate observation of changes in morphology (including cell beating) during culture and require simple and well-established culture systems (such as tissue culture flasks and Petri dishes). An important drawback, however, compared with 3D culture systems, is that monolayer culture is much less similar to the *in vivo* environment, in part because of reduced amount of cell–cell communication and less physiological cell shape. In addition, there is no substitute for 3D culture for

development of tissues for implantation. From the cardiac tissue engineering perspective, therefore, and especially from the standpoint of the biomimetic paradigm, we find 3D culture to be superior to monolayer culture, although monolayer culture provides a very good platform for basic research. In our experience, we have found an iterative combination of experiments performed in monolayer and 3D culture to be best for developing the techniques we present here for cardiac tissue engineering with electrical stimulation.

Microabraded versus unabraded surfaces. In contractile tissues such as myocardium, functional properties are directly related to cellular orientation and elongation. Thus, tissue engineering of a functional cardiac patch critically depends on our understanding of the interaction between multiple guidance cues (e.g., topographical and/or electrical). For studies involving the interactive effects of contact guidance and electrical field stimulation on cell elongation and orientation, we prepare microstructured surfaces on which cells are cultured between stimulating electrodes (Fig. 1). When polyvinyl surfaces are abraded using our protocol, the resulting pattern is V-shaped with a peak-to-peak width of 13 µm and average depth of 700 nm (Fig. 3), which is the ideal size for enhancing the elongation and orientation of neonatal rat cardiomyocytes. For an alternative method for patterning fibroblast



**Figure 2** Generalized protocol flow chart. The steps in this protocol can generally be divided into (i) preparation of the culture chamber (Steps 1–9), (ii) the preparation of either a monolayer culture insert (Step 10A) or a 3D scaffold (Step 10B), (iii) cultivation of cells with electrical stimulation (Steps 11–20) and (iv) assessments of contractile activity (Step 21A), cell alignment/elongation (Step 21B), histology (Step 21C) and ultrastructure (Step 21D). The culture chamber may be prepared ahead of time and stored for future use, but scaffolds or monolayer culture inserts must be ready by the time cells are prepared.

cells using direct-current electrical stimulation, see Box 1.

**Initiation of electrical stimulation.** The effects of electrical stimulation strongly depend on the time of its initiation<sup>8</sup>. If applied too early, electrical stimulation inhibits the accumulation of cardiac proteins and yields poor contractile behavior. If applied too late, electrical stimulation can no longer aid the functional assembly of the cells. For neonatal rat cardiomyocytes seeded with Matrigel into collagen scaffolds, the optimal time to begin electrical field stimulation is after 3 d of cultivation, and the contractile function can be assessed after 8 d (see ref. 8). For cells seeded onto the two-dimensional substrates, electrical stimulation should be initiated 24 h after cell seeding and maintained for an additional 72 h (for a total of 4 d culture time) before the effects of stimulation are assessed<sup>22</sup>.

**Electrical signal parameters.** The electrical signals described in this protocol are designed to mimic those existing in nature under the conditions of interest; living cells are surrounded by a fluid with high electrical conductivity—extracellular fluid *in vivo* (3–12 mS cm<sup>-1</sup>)<sup>29</sup> or culture medium *in vitro* (15 mS cm<sup>-1</sup>)<sup>30</sup>. For vertebrates, the physiologically significant range of endogenous gradients of electrical fields is on the order of 0.1–10 V/cm (see ref. 26).

In terms of frequency, the heart's beating rate can range from 3 to 4 beats per minute (for blue whales during deep dives), up to 360 beats per minute for a rat heart and 1,200 beats per minute for the hummingbird during flight<sup>31</sup>, corresponding to 0.05–20 Hz. In terms of pulse duration, 1–2 ms is sufficiently long to excite heart tissue and cells, and moreover, this signal duration is sufficient also for the double layers on stimulation electrodes to dissipate between subsequent pulses<sup>30</sup> (for further information about the characterization of the electrical stimulation system outlined in this protocol, see **Box 2**). In addition, we have chosen monophasic square-wave pulses for their simplicity and compatibility with carbon rod electrodes. For discussion of customized electrical stimulation systems, see **Box 3**. For discussion of the tradeoffs associated with different waveform shapes, see **Box 4**.

**Pulsatile electrical field stimulation, carbon electrodes.** The main distinction between pulsatile and direct current stimuli is their mechanism of charge transduction. As electrical charges are carried by ions in physiological media and by electrons in electrodes and electrical circuitry, at the electrode–medium interface, there is a transduction of charge carriers from electrons to ions. Charge transfer can occur through three mechanisms: (i) non-Faradaic charging/discharging of the electrochemical double layer,

(ii) reversible Faradaic reactions and (iii) nonreversible Faradaic reactions. The first two mechanisms are desirable, whereas the last should be avoided because it is associated with electrode degradation and harmful byproducts. The relative presence of each mechanism can be assessed using electrochemical impedance spectroscopy (EIS), from which an equivalent circuit of the stimulation system can be constructed (see **Box 2**).

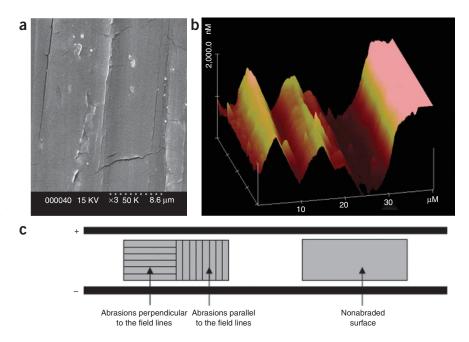
When a stimulus is applied to a physiological medium, a redistribution of charge first occurs, and then, if the stimulus is of long-enough duration, the electrodes will begin to chemically react with the medium to sustain current. A system delivering short stimulation pulses can thus be designed to allow only a tolerable amount of chemical reactions to occur by selecting the electrode properties and pulse characteristics that favor reversible redistributions of charge in the double layer at the electrode-electrolyte interface and reversible chemical reactions<sup>32</sup>. We have found that a square-wave pulse with relatively short-duration (2 ms, or 0.2% of the total cycle) and a relatively long time between pulses, with the carbon electrodes used throughout this protocol,

provides time for the vast majority ( $\sim 85\%$ ) of the processes occurring between electrodes and the electrolyte to reverse<sup>28</sup>. In addition, experimentally, we have also identified a safe stimulation range using carbon rod electrodes with neonatal rat cardiomyocytes, and at this point, we do not recommend stimulation at levels of 8 V/cm and above, although we may refine this range in the future<sup>28</sup>.

In past studies, we have determined carbon electrodes to be the electrodes of choice due to their passive biocompatibility, high availability, low price, superior charge injection characteristics and high resistance to chemical reactions and corrosion<sup>21,30</sup>. In addition, their behavior for a range of electrode configurations (including the ones described in this protocol and others for which the ratio of length of electrode to the spacing between them is greater than 2) resembles that of a parallel-plate capacitor, in which the field gradient is constant between the two conducting surfaces<sup>28</sup> (for more details regarding characterization of electrodes, see **Box 2**).

A system delivering DC stimuli (such as that shown in **Box 1** using Ag/AgCl electrodes which efficiently corrode, providing a steady current) is different than one delivering short pulses, as it necessarily generates chemical byproducts and therefore must be designed to shield the cells from chemical reactions by the use of salt bridges. As the incorporation of salt bridges necessarily adds another level of complexity, these systems are recommended only if the signal of interest generates intolerable amounts of chemical reactions. Electrical characterization of the culture system (**Box 2**) provides information about the mechanisms of charge injection for specific electrodes and input voltages.

The injection of charge from the electrode into electrolyte (culture medium in our case) can be accomplished by either attaching a current source between the two electrodes (that defines



**Figure 3** Setup for simultaneous application of topographical cues and electrical field stimulation. As surfaces abraded with lapping paper of 80-mm grain size (average abrasion width of 13 mm and depth of 700 nm) exhibited the strongest effect on cardiomyocyte elongation and orientation as well as statistically significant effect on orientation of fibroblasts, they were used for electrical field stimulation experiments. (a) Scanning electron micrograph of a polyvinyl coverslip abraded with 80-mm-grain-size lapping paper. (b) Atomic force micrograph of a polyvinyl coverslip abraded with 80-mm-grain-size lapping paper. (c) Orientation of abrasions with respect to the electrodes in the stimulation chamber.

the current to be passed) or applying a voltage source. Although the second method is simpler to implement, it enables only the control of the net potential between the two electrodes, and not of the current, which, rather than voltage, dictates the amount of electrical field applied to the cells. Nonetheless, for pulsatile electrical field stimuli delivered by carbon electrodes, we have found that a voltage-controlled source is sufficient for accomplishing stimulation (for the DC stimulation applied in **Box 1**, however, a current-controlled device is utilized).

#### Ongoing work/future studies

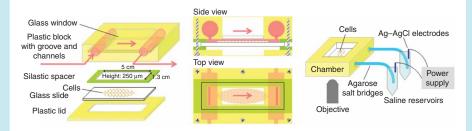
**Optimization of electrical stimulation parameters.** At this point, although we have achieved a remarkable improvement of engineered cardiac tissue with the application of electrical stimulation, optimization of electrical stimulation parameters (including frequency, amplitude and waveform shape) remains an area of future work. To this end, we are developing high-throughput microscale cultures for screening studies involving electrical stimulation.

Assessments. Now that we have progressed to the point of optimizing culture conditions for improving the quality of engineered cardiac tissue, we have found it increasingly necessary to develop advanced assessments of the electromechanical functionality of engineered cardiac tissue. Thus far, for example, we have assessed cell elongation only on monolayer cultures, and so we are now developing methods using confocal microscopy for this purpose. Another shortcoming of our construct evaluation is that it is based on the changes in the construct cross-sectional area: as the construct contracts, its cross-sectional area decreases. However, our method neglects to consider that its thickness may also change.

# **BOX 1 | ENHANCING CELL ELONGATION WITH DC STIMULATION**

Electric-field-induced migration (galvanotaxis) and morphology change (galvanotropism) have been demonstrated in many cultured cell types, such as embryonic cells<sup>33</sup>, corneal fibroblasts<sup>43</sup>, neural crest cells<sup>44</sup> and keratinocytes<sup>45</sup>. In recent studies, we have begun to use *in vitro* systems to apply well-defined DC electric fields to cultured cells to induce an increased level of directional anisotropy, an important feature of native myocardium, in tissue-engineered constructs.

The chamber shown below represents an alternate use for a standard parallel-plate flow chamber used to apply fluid flow over cultured cells on a glass slide. The chamber permits phase or fluorescence monitoring of cell migration. In this modification, the tubing that provides fluid flow into and out of the flow chamber is replaced with two salt bridges that provide a conducting pathway for the applied current. One plate of this chamber consists of a machineable, sterilizable plastic block (such as polycarbonate or polysulfone) with a glass window, whereas a glass slide with cultured cells represents the second plate. The two plates are separated by a uniform-thickness rectangular silastic spacer (McMaster-Carr) with a central rectangular opening, held together with screws and a plastic lid (having a rectangular opening to accommodate the microscope objective), thereby creating a sealed rectangular channel with dimensions of 5, 1.3, 0.250 cm (length, width and height or gap distance, respectively). This sealed chamber has been originally designed for short-term studies and has been used for up to 3 h with up to 40,000 cells at 3 mA without observable color changes of the phenol red medium. For longer-term studies, however, a slow-medium perfusion and/or use of gas-permeable spacers (with placement of the setup in an environmental chamber) can be incorporated into the system to maintain gas exchange.



The well-defined chamber geometry permits application of a prescribed electrical field strength or current density. Two salt bridges prevent electrolysis products from contaminating the chamber by providing a pathway for current from each media reservoir to an Ag–AgCl electrode (one positive: anode, and one negative: cathode). Salt bridges are prepared from flexible plastic tubing filled with 2% agarose in PBS. This chamber is ideally suited for DC stimulation because of its well-defined geometry. However, to attain voltages in the physiological range, high voltage levels are needed to overcome high electrical resistance of system. In addition, because of corrosion of the silver/silver chloride electrodes, the electrical resistance of the system is constantly changing, necessitating a current-controlled system. We recommend the Keithley SourceMeter 2410.

#### Salt bridges

1. Make 2% wt/vol agarose by mixing 50 ml of PBS with 1 g of agarose, heat in the microwave until the agarose dissolves, about 2–3 min. Let agarose cool until safe to touch.

2. Use a syringe and fill tubing (45 cm long, 1.8 mm inner diameter) with agarose and permit gelling of the agarose. *Note*: any bubble formation in the tubing could obstruct the current flow; therefore, it is very important to avoid all bubbles. It is also advisable to overfill the tubing, as agarose may shrink slightly when cooled.

**PAUSE POINT** Agarose salt bridges can be fabricated and stored in PBS at RT until use (up to 1 month).

#### Electrodes

Partially soak silver wire (0.6 mm diameter, 5 cm long) in bleach (Clorox) for 10 min to make Ag-AgCl electrodes. Short pairs of electrodes together (using wire with gator clips) to minimize mismatch due to polarization effects.

#### Chamber

Clean/sterilize galvanotaxis chamber assembly parts with an ethanol wipe and air-dry in sterile hood.

1. Wearing sterile gloves, put one gasket into the groove of the chamber, being careful not to occlude the flow slits on each end of the flow channel. For 3D stimulation, the thickness of this gasket will determine the thickness of construct that can be placed in the chamber.

2. Add 0.5 ml of medium on the glass window of the galvanotaxis chamber within the gasket.

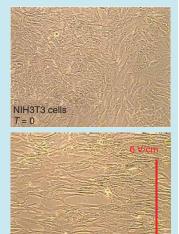
3. Place the slide (cell side down) into the chamber by positioning one end of the slide into the groove first and slowly lowering the other side until the slide is flush with the chamber. The interior region of the gasket (i.e., flow channel) should now be completely filled with media. Be careful not to shear the cells.

4. Put another silicone spacer (to cushion the plastic lid) on top of the slide and then position the plastic lid and secure with screws. Screws should be tightened in alternating sides of the chamber to maintain balance and prevent cracking of the glass slide.

5. Fill the two reservoirs with media. Both ends of each reservoir are tapered to fit a male luer stopcock. Fill chamber reservoirs (one at a time) with medium using a syringe and appropriate stopcock configuration (open or closed) and luer plug. When filling a given reservoir, make sure that the other reservoir is sealed shut. Tap lightly to remove air bubbles. The entire chamber should now be filled with media.

6. Connect the salt bridges to the chamber through the luer connectors. Place chamber upside-down from the assembling orientation so that the cells are facing up. Open the stopcocks. Place the other end of the salt bridges in PBS reservoirs. Place silver electrodes in the PBS reservoirs and connect with the power source. *Electrical stimulation* 

- 1. Allow cells to attach to slide for 12–18 h (for 3T3 cells).
- 2. Set current to 3 mA to apply an electric field of 6 V/cm.
- 3. Take brightfield images once every 10 min to monitor the elongation (perpendicular to the electric
- field) and movement of cells (as shown in images on the right).



T = 3 h

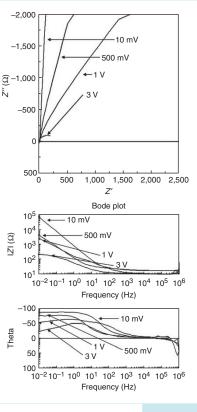
# **BOX 2 | CHARACTERIZING ELECTRICAL STIMULATION SYSTEMS**

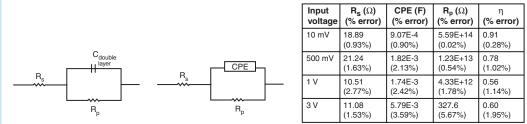
#### Electrochemical impedance spectroscopy

Electrochemical systems such as the stimulation systems described here are nonlinear, and so are therefore more difficult to characterize than electrical systems composed of linear circuit elements (such as resistors and capacitors). As mentioned elsewhere in this protocol, charge transfer between electrodes and culture medium can occur through three mechanisms: (i) nonFaradaic charging/discharging of the electrochemical double layer, (ii) reversible Faradaic reactions and (iii) nonreversible Faradaic reactions. The first two mechanisms are desirable, whereas the last should be avoided because it is associated with electrode degradation and harmful byproducts. The relative presence of each mechanism can be assessed using EIS, from which Nyquist plots (real versus imaginary parts of impedance) and Bode plots (impedance versus frequency) of the stimulation system can be constructed, as shown to the right (in this case, for 1/8-inch-diameter carbon rod electrodes measured with increasing input voltages).

#### Equivalent curcuits

To provide insight into the behavior of the system being analyzed, the elements in the model should have a basis in the physical electrochemistry of the system. The figure below (left), for example, shows the equivalent circuit for a simple electrochemical cell, in which R<sub>s</sub> represents the resistance of the bulk solution, R<sub>p</sub> represents the polarization resistance, which is the electrode's resistance to corrosion and C<sub>double-layer</sub> represents the capacitance of the double layer of charge induced by the accumulation of electrons on the electrode and the corresponding accumulation of ions in the solution in proximity to the electrode. In practice, the double layer-capacitance is often replaced by a 'constant-phase element' (CPE), as shown in the figure below (middle), which describes a nonideal capacitor (with ideality coefficient  $\eta$  ranging from 0 to 1 with increasing ideality). A table of calculated equivalent circuit parameters is shown in the figure below (right).





In our laboratory, EIS measurements are taken with an electrochemical interface (Solartron 1287) and a frequency response analyzer (FRA, Solartron 1250) controlled by a computer with ZPlot software. Equivalent circuits and associated parameters are determined using ZView 2.5b. 1. Take EIS measurements of electrodes in 60-mm Petri dish with 20 ml of PBS.

- 2. Acquire EIS spectra over a frequency range of  $1 \times 10^6$  to  $1 \times 10^{-2}$  Hz with a range of perturbation values.
- 3. Record for each frequency the real (resistive) and imaginary (capacitive) components of the impedance response, Z' and Z", respectively.
- 4. Evaluate data in ZView to generate Nyquist and Bode plots for each condition.
- 5. Create an 'equivalent circuit' of the system using resistors and capacitors in series and in parallel.

6. Calculate the values for CPE (constant-phase element, a measure of capacitance),  $R_p$  (polarization resistance: a measure of resistance to chemical reactions) and  $\eta$  (a term, ranging from 0 to 1 to describe the 'ideality' of using instant fit functions in ZView software). An example of EIS analysis of carbon at different perturbation voltages is shown above. The data above indicate that as the input voltages increase, although the capacitance (CPE) increases, the resistance to chemical reactions ( $R_p$ ) decreases, and so we are motivated to minimize input voltages whenever possible.

In addition, by using an electrical field stimulus to perform this assay, the effects of cell-to-cell coupling cannot be separated from the changes in amplitudes of contractions of individual cells. Furthermore, as the application of suprathreshold electrical stimulation causes contraction of cells, which in turn yields mechanical directionality cues, we would like to decouple these effects in future studies. For these reasons, we believe that, going forward, a stronger measurement of contractile function is that of its generated force, and we are in the process of developing these assays. In addition, quantifying impulse propagation will also be crucial for understanding the level of electrical coupling of the cells in the engineered cardiac tissue and determining the presence of any arrhythmia. Finally, *in vivo* assessments will be essential for determining the utility and functional integration of our engineered cardiac constructs, and we are in the process of performing these.

# **BOX 3 | CUSTOM ELECTRICAL STIMULATION SYSTEMS**

In addition to commercially available electrical stimulation systems (Grass and so on), our laboratory also uses custom computer-controlled systems. These offer more control and more stimulation channels at a favorable price. We have two primary systems.

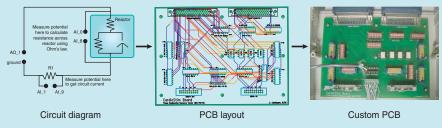
- Stimulation only: moderate cost board with multiple analog output channels (8–32).
- Stimulation with simultaneous potential measurement: more expensive board with four analog output channels and 32 analog input channels.

#### Computer/data acquisition board

- 1. Almost any modern computer is sufficient for data acquisition, provided it has at least one free PCI slot.
- 2. Data acquisition (DAQ) boards. Our laboratory uses the following from National Instruments.
  - (a) Stimulation only: PCI 6723 with 32 analog output (~\$1,000). Maximum current of 20 mA per channel.
  - (b) Stimulation and measurement: PCI 6289 with 32 analog inputs and 4 analog outputs (\$1,700). Maximum current of 20 mA per channel.

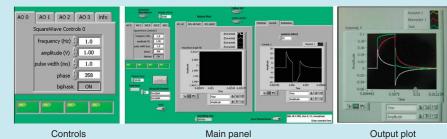
#### Interface

Here there are several choices, from the most basic using a purchased I/O connector block ( $\sim$ \$100), to a moderate solution of using a bread box with connector block, to the most advanced of designing a custom-printed circuit board (PCB,  $\sim$ \$300). The connector block or PCB should be connected to DAQ board with a shielded cable. The figures below are for a custom PCB that we designed for our electrical stimulation and measurement system. At each of the four channels, the potential is measured across a resistor (R1) to get circuit current, and across a bioreactor whereby resistance change as a function of time may be calculated using Ohm's law. Optically isolated digital relays are used to maintain channel independence.



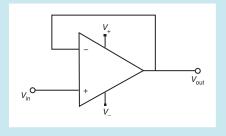
#### Programming

While there are numerous programs available for data acquisition and control, LabView from National Instruments offers a good balance of advanced features and relative ease-of-use. Common waveforms (square, sawtooth and so on) exist as built-in functions. Unique waveforms are easily programmed, or may even be drawn on screen. Screen shots below are from the program that we use for electrical stimulation and measurement.



#### Amplification (optional)

As the maximum current rating of the employed card is only 20 mA, if our application requires a higher current rating, we use operational amplifier wired in unity-gain mode, as shown in the figure to the right. The specific chip we use is the OPA-551 from Burr-Brown, chosen for its high current rating (200 mA), high voltage range (-12 V through +12 V) and stability in unity-gain configuration.

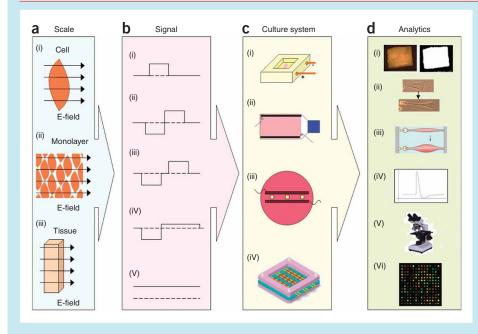


#### MATERIALS REAGENTS

## Cell culture

- Matrigel (Becton Dickinson, cat. no. 356234) (sterile) ▲ CRITICAL Basement membrane matrix contains many undefined components and we have not tested matrices from other suppliers.
- · Bovine fibronectin (Sigma, cat. no. F1141) (sterile)

- •95% (vol/vol) ethanol (Pharmco, cat. no. 111000190)
- Carboxyfluorescein diacetate, succinimidyl ester (CFDA; Molecular Probes, cat. no. C-1354) (nonsterile)
- Propidium iodide (PI) (Invitrogen, cat. no. P1304MP) (nonsterile)
- **! CAUTION** PI is a potential carcinogen. Material may cause irritation to the skin, eyes, mucous membranes, and the upper respiratory tract. When



# **BOX 4 | GUIDELINES FOR FUTURE STUDIES**

The figure to the left shows an overview of some additional experimental parameters that may be varied for electrical stimulation, including (a) the biological scale, which ranges from (i) single cells and (ii) monolayers to (iii) tissue; (b) the electrical signal, including (i) monophasic pulses, (ii) charge-balanced biphasic pulses, (iii) charge-balanced biphasic pulses with interphase delay, (iv) chargebalanced biphasic pulses with slow reversal and (v) direct current; (c) the culture system, including (i) a chamber complete with salt-bridges to shield cells from stimulation, (ii) an outfitted T-flask, (iii) an outfitted Petri-dish and (iv) a customized culture chamber and (d) the analytics, which may be performed to determine (i) contractile activity, (ii) elongation, (iii) force of contraction, (iv) electrical activity, (v) morphology and (vi) gene expression.

When planning cell culture experiments involving electrical stimulation, factors to consider include the duration and shape of the stimulus waveform, the type and size of the biological specimen, the electrical property being exploited, the duration of the experiment (minutes to hours to weeks) and the electrode configuration and properties required for the particular bioreactor setup.

*Choosing a biological scale* Different biological scales are appropriate for different types of studies. In terms of cardiac tissue engineering, studies involving the quantification of cell migration and/or elongation as well as visualization of cell beating may be best performed on sparse populations of cells so that changes in cell shape may be monitored and cell position may be tracked. Cell-patterning applications, however, or studies in which larger populations of cells are needed, may call for monolayers of cells, or even 3D cultures, which are necessary for implantation applications.

*Choosing an electrical signal* This choice depends not only on the type of physiological signal you are mimicking but also on the considerations involving the amount of electrochemical reactions involved in generating the electrical stimulus. Some mitigation of the amount of charge converted to chemical reactions may be decreased by roughening the surfaces of stimulating electrodes, whereby electrode surface area is increased and the current density is reduced. The application of biphasic pulses (b(ii) above) is another way to counteract some of the irreversible reactions that the electrodes produce at the interface with culture medium. However, the immediate injection of a secondary pulse, although aiding in achieving a higher level of reversibility, can interfere with the initiation of an action potential. Delaying the secondary pulse (b(iii) above) or slowing down the time for charge reversal (b(iv) above) helps lessen this effect. Customized electrical stimulation systems (**Box 3**) allow for the application of the above types of signals, as well many others.

*Choosing culture system* Design considerations are interdependent and include the duration and shape of the stimulus waveform, the size of the tissue construct in question, the electrical property being exploited (e.g., generation of reactive oxygen species versus eliciting action potential), the duration of the experiment and the mechanical properties required of the electrode in the bioreactor setup. The three main modifications shown in part c of the figure above (c(iii) being described in the main protocol here) include a modified flow chamber with shielded electrodes, standard culture flasks, and a customizable culture chamber. The systems most suitable for studies on the effect of pulsatile electric field stimulation on cultured cells are shown in c(ii) and (iii) because they are simple to use and simple to construct; the electrodes are simply fitted directly into standard culture flasks and Petri dishes, respectively. For screening studies, as well as for studies involving cells or medium that are particularly rare and/or expensive, it may be desirable to minimize cell culture volume. For these applications a customized electrical stimulation culture chamber is required (c(iv)). In this instance, the small diameter (<1.6 mm) of electrode rod requires an electrode material with good mechanical properties.

*Choosing analytics* The choice of analytics mostly depends on the biological scale and culture system. Amplitude (d(i)) and force (d(ii)) of contractions may be performed most easily, e.g., on 3D tissues (a(iii)), which are best stimulated in an outfitted Petri dish (c(iii)), whereas changes in cell elongation (d(i)) may be best performed on sparse cell populations (a(i)), stimulated in either an outfitted T-flask (c(ii)) or DC chamber (c(i)).

handling, wear chemical resistant gloves and chemical safety goggles, and handle only under a fume hood with adequate ventilation.

- N-2-hydroxyethylpiperazine-N'-2-ethane-sulfonic acid (CellGro, cat. no. 25-060-cl)
- Penicillin (GIBCO, cat. no. 15140)

Histological analysis

• 10% (vol/vol) buffered formalin (Sigma, cat. no. 533998) **! CAUTION** Formalin is toxic, allergenic and carcinogenic. Handle only under a chemical fume hood.

<sup>•</sup> High-glucose DMEM, 4 g ml $^{-1}$ , with L-GIn, without sodium pyruvate (Invitrogen, cat. no. 11965)



- Horse serum (Vector Laboratories, cat. no. S-2000) (nonsterile)
- Tween 20 (Sigma, cat. no. P7949) (nonsterile)
- · Mouse anti-cardiac troponin I (TnI; Millipore, cat. no. AB1627) (non-sterile)
- Rabbit anti-connexin 43 (Cx43; Millipore, cat. no. AB1728) (nonsterile)
- ▲ **CRITICAL** This antibody is specific for Cx43; not reactive with other connexins.
- Texas-Red-conjugated horse anti-mouse IgG (Vector Laboratories, cat. no. TI-2000) (nonsterile)
- Fluorescein-conjugated goat anti-rabbit IgG (Vector Laboratories, cat. no. TI-1000) (nonsterile)
- •4,6-Diamidino-2-phenylindole (DAPI) mounting medium (Vector
- Laboratories, cat. no. H-1200)

#### Ultrastructure analysis

- Sodium cacodylate trihydrate (Sigma-Aldrich, cat. no. C4945) **! CAUTION** Toxic, handle only under a chemical fume hood.
- Reagent grade, crystalline paraformaldehyde (Sigma-Aldrich, cat. no. P6148) • CAUTION Toxic, handle only under a chemical fume hood.
- Gluteraldehyde, grade I, 8% (vol/vol) in H<sub>2</sub>O, specially purified for use as an electron microscopy fixative or other sophisticated use, pH = 7.4 (Sigma-Aldrich, cat. no. G7526) **!** CAUTION Toxic, handle only under a chemical fume hood.
- Epoxy embedding kit (Epon 812, SPI Supplies)
- 1% Osmium tetroxide, ReagentPlus, 99.8% (Sigma-Aldrich, cat. no. 201030) **! CAUTION** Osmium tetroxide is highly toxic and a rapid oxidizer. Handle with care under a chemical fume hood.
- $\cdot$  (±)-Propylene oxide, Reagent Plus, 99% (Sigma-Aldrich, cat. no. 110205) **EQUIPMENT**
- Inverted or noninverted microscope (e.g., Olympus, cat. no. CK40)
- Stereomicroscope (e.g., Olympus, cat. no. SZ2-LGR)
- Oscilloscope (with option to save waveforms, e.g., Tektronix, cat. no. TDS3014B)
- Electrical stimulator (providing a sufficient amount of current, e.g., Grass Technologies s88x dual output stimulator with 600 mA current rating)
- Ultrasound cleaner (e.g., Misonix, cat. no. 1510R-MT)
- Digital multimeter (with capability to test for short-circuits, e.g., Extech true RMS digital multimeter, RadioShack)
- Video camera (with at least 30 frames per second, e.g., CFM-USB-4 from Angstrom Sun Technologies)

- Class II biosafety cabinets
- CO<sub>2</sub> incubators (Napco, Thermoelectron)
- ·Heated microscope stage (e.g., ThermoPlate MATS-U4020WF)
- Leica Ultracut UCT
- Computer that can run MATLAB Version 7.0 (i.e., with DVD drive, 512 MB RAM or higher, 600-MB disk space and Internet access)
- Culture chamber
- No. 80 size drill Bits (nonsterile)
- •GE RTV (room temperature vulcanization) 108 silicone adhesive (nonsterile)
- Needlenose pliers (nonsterile)
- Graphite electrodes (Ladd Research Industries, 1/8-inch diameter, cat. no. 30250) (nonsterile)
- Platinum wire (Ladd Research Industries, 8 mil, cat. no. 30572) (nonsterile)
- Color-coded alligator test leads (Radio Shack, cat. no. 278-1157) (nonsterile)
- •Electrical resistors (Mouser) (nonsterile)
- •60-mm glass Petri dish (e.g., VWR, cat. no. 89000-318) (nonsterile) Cell culture
- •6-well polystyrene plates (sterile)
- Collagen sponge scaffolds (Ultrafoam, Davol, cat. no. 1050050) (sterile)
- •Kim wipes (Fisher, cat. no. NC9777000) (sterilized by autoclaving)
- Sterile gloves (Fisher, cat. no. 11-388-128G)
- Alcohol wipes (Fisher, cat. no. 06-669-62)

#### Microabraded surfaces

- 80-µm aluminum oxide lapping paper (McMaster-Carr, cat. no. LPA80) (nonsterile)
- Poly(vinyl) coverslips (VWR, cat. no.; 48376-049) (nonsterile)
- Laboratory labeling tapes (VWR, cat. no. 36428-065) (nonsterile) REAGENT SETUP
- Cardiac culture medium (sterile), comprised of: high-glucose DMEM + 10% (vol/vol) heat-inactivated fetal bovine serum, 1% (vol/vol) N-2hydroxyethylpiperazine-N'-2-ethane-sulfonic acid, 1% (vol/vol) penicillin.
- Can be stored at 4 °C for not longer than 3 weeks. **! CAUTION** Prepare under a biological hood.
- •Karnovsky's reagent: 0.1 M sodium cacodylate with 2% (vol/vol) paraformaldehyde and 2.5% (vol/vol) gluteraldehyde, pH = 7.4. Can be stored at 4 °C for not longer than 2 weeks. **!** CAUTION Prepare under a chemical hood.

# PROCEDURE

#### Culture chamber preparation $\bullet$ TIMING $\sim$ 3 h

**1** Cut two carbon electrode rods to appropriate lengths: for a 60-mm diameter dish, cut them to a length of 5.7 cm, for a 100-mm diameter dish, cut to a length of 9.7 cm. Cut two 7-cm pieces of platinum wire.

**2** Place drill bit into the tip of the drill and drill two holes 2 mm apart from each other through each electrode, as close to the end of the electrode as possible,  $\sim 2$  mm from the end, as shown in **Figure 1c**. As we will cover this connection with silicone in Step 8, the closer the connections are to the edges of the electrode, the more space will be available between the electrodes for cell culture.

**3**| Thread the platinum wire through the hole closer to the middle of the electrode, allowing no wire to poke through the other end, as shown in **Figure 1c**. Wrap the platinum wire around the electrode, and thread through other hole. Pull tightly to create a good connection from the platinum wire to the electrode, but at the same time, be careful not to snap the electrode. The amount of wire hanging off the electrode should be enough to reach out of the bioreactor with just enough room for connectors you will be using to connect to it.

▲ **CRITICAL STEP** Free wire ends allow easy electrical connection between the electrical stimulator and the bioreactor, and they need to be easily attached and detached for medium changes, but because they are not insulated, the free wire ends should not be excessively long, just long enough to connect an alligator clip.

4 Squeeze two strips that are 1.1 cm long of RTV silicone adhesive to the bottom of the Petri dish, at opposing ends, as shown in **Figure 1b**.

**5**| Press the electrodes into the adhesive at the bottom surface of the dish. Be careful to avoid getting any adhesive on the sections of the electrodes that will face the cells (as shown in **Fig. 1c**) because silicone is an insulating material that will block the delivery of the electrical field stimulus. For use with monolayer inserts (which will be 8 mm  $\times$  10 mm), space the electrodes so that there is 1 cm from the edge of one rod to the other (for purposes of calculating electrical field with this configuration, divide input voltage by 1.1 cm)<sup>28</sup>. For use with 3D constructs (which will be 6 mm  $\times$  8 mm), space the electrodes so that there

is 1 cm spacing from the center of one rod to the center of the other (for purposes of calculating electrical field with this configuration, divide input voltage by 1.0 cm)<sup>28</sup>. It is also important to make sure that the attached wires should be on opposite sides of the opposing electrodes as shown in **Figure 1b,c**. This placement of wires balances the effect of electrode resistance and ensures that a uniform amount of electrode resistance will be encountered for any given current path through the system. Allow silicone to set for 20 min in a 60 °C oven.

▲ **CRITICAL STEP** It may help to place the Petri dish on top of a piece of graph paper with 1-cm spacing to aid in proper electrode placement.

**6** Wipe off the probes of a digital multimeter with an alcohol pad and allow to dry. Using the 'short circuit' option, check that there is a short circuit between the tip of the wire furthest from the Petri dish and electrode, which means you have made a good electrical connection. Also check by caliper that the electrode spacing has not changed while the silicone was setting. If it has, use a scalpel to scrape all silicone from the bottom of the dish and start over with new electrodes.

▲ **CRITICAL STEP** If electrodes are improperly aligned, the electrical field gradient will be greater where electrodes are closer together, and lesser where they are further apart.

# ? TROUBLESHOOTING

7| Now that the electrodes are securely fastened to the bottom of the dish, prebend the platinum wire so that it comes out of the Petri dish neatly—this will also facilitate placing the Petri dish lid over the chamber. Also keep in mind that bending the delicate platinum wire too much may cause it to snap.

8 Squeeze another strip of silicone adhesive over the exposed platinum wire twisting around the electrode, as shown in Figure 1d.

**9** Repeat this procedure to prepare the desired number of culture chambers (you will be able to accommodate four 3D scaffolds or three monolayer inserts in a 60-mm chamber, and six scaffolds or four monolayer inserts in a 100-mm chamber). If you are planning to perform assessments of contractile activity (Step 21A), make an extra chamber to allow testing of individual constructs in Step 21A(ii). Autoclave culture chambers in sealed autoclave bags for 20 min on dry cycle (the silicone adhesive will set in the autoclave).

■ **PAUSE POINT** The culture chambers may be stored in their autoclave bags for up to 3 months in a dry place at room temperature (RT; 18–25 °C).

# Preparing cells for culture • TIMING 12-18 h

**10** Prepare cells for culture (using our previously published cell-isolation protocol)<sup>27</sup> and seed them either in a monolayer (unpatterned or patterned; using option A) or a 3D scaffold (option B).

# (A) Preparing cells on monolayer surface $\bullet$ TIMING $\sim$ 30 h including sterilization

- (i) (Skip this step for unpatterned surface.) Cover one-half of your polyvinyl carbonate coverslips (22 mm × 22 mm) with laboratory tape and use lapping paper to abrade one-half of the coverslip in one direction (~30 strokes should provide good abrasions). Peel off the tape, cover the part of the coverslip just abraded and abrade the other half of the coverslip in the orthogonal direction to observe the cells' response to two different topographical cues on the same coverslip. Observe under the microscope that the abrasions are straight (i.e., that all are running in the same direction in a particular area and not crisscrossing due to accidental scratches).
- (ii) Cut the abraded coverslips into 8 mm  $\times$  22 mm rectangles. Be careful that you cut the strips so that both directions of abrasions are included in the strip, and not that you are cutting a strip entirely out of a piece of the coverslip abraded in only a single direction.
- (iii) Wearing tight-fitting gloves (for better control) fold along the two shorter edges by hand to form a 'table' with a surface of 8 mm  $\times$  10 mm and cut the 'legs' to a height of 1.5 mm (to ensure that the cells cultured on the coverslips are placed at the identical height in the center between the carbon electrodes used for electrical stimulation).
- (iv) Remove particulate debris by sonicating the surfaces in soap and water followed by rinsing in distilled water.
- (v) Sterilize the surfaces in 95% (vol/vol) ethanol for 24 h, followed by drying and UV irradiation for 30 min at RT (25 °C).
- (vi) For cardiomyocyte culture, coat the surfaces at RT for 2 h with 25  $\mu$ g ml<sup>-1</sup> of bovine fibronectin in phosphate buffered saline (PBS) to enhance cell attachment (60  $\mu$ l of solution per coverslip).
- (vii) Pipette off the excess fibronectin.
- (viii) Resuspend cells at the desired cell density such that there are 500,000 cardiomyocyte cells per 60 μl. Then pipette 60 μl of this suspension onto each coverslip and incubate them in a 100-mm Petri dish at 37 °C/5% CO<sub>2</sub> for 1 h. After 1 h, fill the chamber with 20 ml of culture media.
  ? TROUBLESHOOTING

# (B) Preparing cells in 3D scaffold • TIMING ~ 3.5 h

- (i) Under a laminar flow hood, wearing sterile gloves, cut the collagen scaffold into rectangles 6 mm  $\times$  8 mm  $\times$  1.5 mm.
- (ii) Immediately before use, hydrate each collagen scaffold in culture medium for 2 h in a 37  $^{\circ}C/5\%$  CO<sub>2</sub> incubator.
- (iii) Collect cells by centrifugation at 200*g* for 10 min at 4 °C and resuspend in liquid Matrigel using 5 μl Matrigel per 1 million cells, while working on ice to prevent premature gelation.

- (iv) Gently blot dry prewetted collagen scaffolds on a sterile Kimwipe (autoclaved previously), and then pipette cell suspension in Matrigel evenly on the top surface of each scaffold. Inoculate each scaffold with 30  $\mu$ l of the freshly isolated heart cells–Matrigel suspension (density of  $1.35 \times 10^8$  cells cm<sup>-3</sup>). Place each inoculated scaffold into a single well of a 6-well plate and place in a 37 °C, 5% CO<sub>2</sub> incubator.
- (v) Gelation is complete within 15 min in a 37 °C incubator. Add 4 ml of warmed culture medium to each well of the 6-well plate and keep in culture until ready for use.

# Assemble culture chamber • TIMING 30 min

11 Culture chamber should be assembled according to option A for monolayer culture or option B for 3D construct culture.

# (A) Culture chamber assembly for monolayer culture

(i) With sterile forceps, place coverslips (prepared in Step 10A) between the electrodes in the chamber (prepared in Steps 1–9) (see Fig. 1g) with the table legs orthogonal to the electrodes (the way the 'tables' were made should ensure that when they are placed in between the electrodes, half of any abrasions will be parallel and half will be orthogonal to the electrical field). Figure 3c is an example with two coverslips. Four 'tables' may fit in a 100-mm diameter dish, and three in a 60-mm dish.

# (B) Culture chamber assembly for 3D construct culture

(i) With sterile forceps, place scaffolds (prepared in Step 10B) between electrodes in culture chamber (prepared in Steps 1–9) (see **Fig. 1f**). Place four scaffolds in the chamber—six should fit in a 100-mm diameter dish, and four in a 60-mm dish.

**12** Add 15 ml of cardiac medium to 60-mm Petri dish or 25 ml to a 100-mm dish, making sure there is enough culture medium to cover the electrodes to ensure proper current flow. Cover and place chamber onto the lid of a 150-mm diameter plastic Petri dish to facilitate carrying, and to provide an insulating layer between the dish and the metal incubator shelves. Place in incubator (37  $^{\circ}$ C, 5% CO<sub>2</sub>) and culture for 24 h before applying electrical stimulation to monolayer culture inserts, or for 3 d in the case of 3D constructs.

▲ **CRITICAL STEP** Do all this while paying particular attention to preventing constructs from floating out from between the electrodes.

# ? TROUBLESHOOTING

# Apply electrical stimulation • TIMING 30 min

**13** Connect a red alligator test lead to one platinum wire (this will be connected to the 'positive' wire from the electrical stimulator) and a black alligator test lead to the other platinum wire of your culture chamber (this will be connected to the 'negative' wire from the electrical stimulator). Keep track of which electrode is your 'positive' electrode and which is your 'negative' by labeling the culture chamber. Gently pull the ends of the test leads outside the incubator and secure them with tape so that they do not move when the incubator door is opened and closed. Close the incubator door, and connect the positive output of the stimulator to the red alligator test lead and the negative output of the stimulator to the black alligator test lead. **A CRITICAL STEP** Make sure the stimulator is turned off when performing this step. Take care to prevent any undesired electrical connections (such as accidentally touching wires to metal incubator trays, or allowing platinum wires from adjoining bioreactors to come into contact). If you connect more than one bioreactor to a single channel, make sure not to surpass the current limit of your electrical stimulator. Use the following calculation to see how many bioreactors your system allows in parallel:  $I_{max} = X \times V_{stim}/R_s$ , where  $I_{max}$  corresponds to the current limit of the electrical stimulator, X is the number of bioreactors you intend to connect in parallel,  $V_{stim}$  is the amplitude of the applied voltage and  $R_s$  is the resistance of the bulk solution in your bioreactor (for electrodes spaced at a 1-cm distance, with a length of 5.7 cm (out of which 4 cm is exposed to the culture medium), we have measured  $R_s = \sim 10 \text{ ohms}$ )<sup>28</sup>.

14 Apply monophasic pulses by following option A for monolayer cultures and option B for 3D scaffolds.

# (A) Application of monophasic pulses to monolayer cultures • TIMING 3 d

- (i) For cells seeded onto monolayer surfaces (either abraded or unabraded), start electrical stimulation 24 h after seeding monolayer cultures.
- (ii) Stimulate with 1-ms duration square pulses delivered at 1 Hz and amplitude of 5 V.
- (iii) Keep cells in culture in a 37 °C, 5% CO<sub>2</sub> incubator, and replace the culture medium 100% every other day. Stop electrical stimulation 4 d after seeding (3 d of electrical stimulation).

# (B) Application of monophasic pulses to 3D scaffolds • TIMING 5 d

- (i) Start electrical stimulation 3 d after seeding scaffolds.
- (ii) For scaffolds of cardiomyocytes seeded with Matrigel, stimulate with 2-ms duration square pulses delivered at 1 Hz and amplitude of 5 V.
- (iii) Keep 3D constructs in culture in a 37 °C, 5% CO2 incubator, and replace the culture medium 100% every other day. Stop electrical stimulation 8 d after seeding scaffolds (5 d of electrical stimulation).
  ? TROUBLESHOOTING

# Check electrical stimulation in culture chamber • TIMING 30 min

**15** To allow measurement of the current in the culture chamber during electrical stimulation (Step 14), construct a circuit by placing a 10-ohm resistor ( $R_m$ ) in series with the bioreactor in the stimulation loop as shown in **Figure 4a**.

**CRITICAL STEP** The value of this resistor should be large enough to be able to read a potential drop across it during a stimulus, but as small as possible. For the bioreactor outlined in Steps 1–9, we choose a 10-ohm resistor.

# ? TROUBLESHOOTING

**16** The amount of current flowing through the bioreactor is calculated simply by measuring the potential drop across the resistor, and recording over time the voltage across the resistor with the oscilloscope. For each desired time point measured on the oscilloscope, calculate the value of current by dividing the measured voltage across the resistor by the resistance value  $R_m$  (Ohm's law I = V/R where V is the voltage measured with the oscilloscope, I is the current and R is the resistance). **? TROUBLESHOOTING** 

17| With an oscilloscope, measure the voltage of the source before and after bioreactors are attached (Fig. 4a). Compare the waveforms, and check that the intended waveform is faithfully applied to the bioreactor (an example of this is shown in Fig. 4b). If not, the current limit of stimulator may be exceeded and may need to be increased (see **Box 3** for building custom-stimulation devices). **? TROUBLESHOOTING** 

**18** (Optional) If you are interested, calculate the total amount of injected charge by integrating the current profile for the duration of the stimulus with computational software (e.g., EXCEL, MATLAB or SigmaPlot software). We have done this for a variety of electrode types, including carbon, titanium, stainless steel and titanium nitride-coated titanium, and determined carbon to be the material with the highest amount of injected charge<sup>30</sup>.

**19** (Optional) If you are interested in assessing the amount of charge that is irreversibly delivered in your system, integrate the current profile with computational software (e.g., EXCEL, MATLAB or SigmaPlot). Include not only the stimulus, but continue for several ms further until a current of 0 is reached (i.e., during the reversal of all reversible chemical processes).

**20** Monitor the currents every day during culture and note any significant changes, which may be a sign of corrosion of electrodes/detached wire and so on.

# Assessments of the engineered cardiac tissue

**21** Assessments of the engineered cardiac tissue can be carried out using the following options: option A for assessment of the contractile activity of engineered cardiac constructs; option B for end-point assessment of cell alignment and elongation of cell monolayers; option C for end-point histological analysis (including analysis of gap junctions); and option D for end-point ultrastructural analysis.

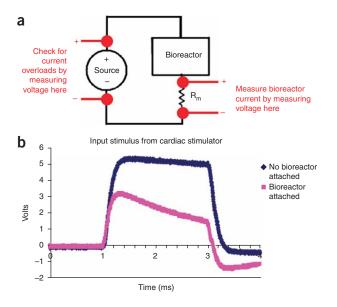
# (A) Assessment of the contractile activity of engineered cardiac constructs • TIMING 1 h setup/cleanup + 10 min per construct

(i) Assess contractile activity of live engineered cardiac constructs visually by measuring contractile activity in response to electrical field stimulation. If this is an end-point analysis, there is no longer a need to maintain sterility, but otherwise, this procedure should be performed under a biological hood. In addition, we recommend the use of a microscope-incubator system, if available, to guarantee proper temperature and pH.

▲ CRITICAL STEP If a microscope-top incubator is not available, prepare a solution of Tyrode's salts (Sigma) according to the manufacturer's instructions and warm to 37 °C (Tyrode's solution provides some pH buffering and should be replaced for each new construct measured).

(ii) Connect a new 60-mm diameter culture chamber prepared in Steps 1–9 to a cardiac stimulator (either Grass S88X or custom system) and fill with 15 ml of warmed Tyrode's solution. We use a new culture chamber here because we measure each construct individually, and all other constructs may remain in the incubator while we are performing measurements.

**Figure 4** | Checking electrical stimulation. (a) An equivalent circuit of setup for checking electrical stimulation. To check the current, connect a measurement resistor Rm in series with the bioreactor, measure the voltage across it and back-calculate the current (assumed to be the same as that through the bioreactor, given Kirchoff's current law) using Ohm's Law (V = IR), where V is the voltage, I is the current and R is the resistance of a voltage loop. To check that the current limit of the stimulation device is not surpassed by attaching the bioreactors to it, measure voltage of the source before and after the bioreactors are attached and compare waveforms. (b) Stimulus waveform from commercial stimulator with low current rating. When a bioreactor is attached (pink), the stimulus waveform (blue) is no longer faithfully applied. Either too many bioreactors are hooked up in parallel to this channel, or the current rating of your stimulation device is too low. In this case, a custom stimulator may need to be built (see **Box 3**).

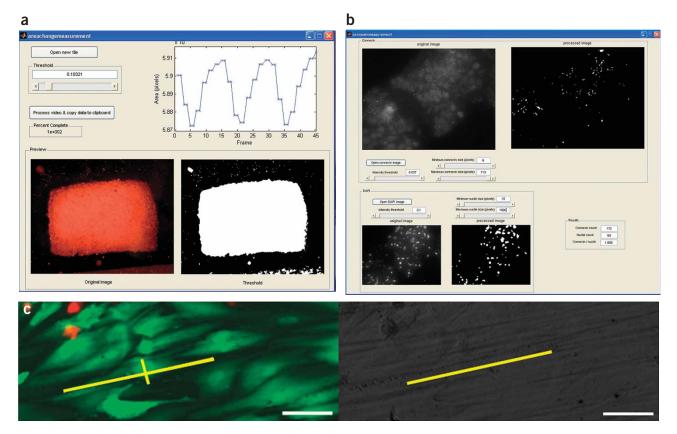




- (iii) Maintain the temperature of the Tyrode's solution at 37 °C by placing the Petri dish on top of a heated stage.
  ▲ CRITICAL STEP Cardiomyocytes are very sensitive to temperature variations, so it is critical to maintain temperature or else all measurements will be compromised.
- (iv) Place the entire setup on an optical microscope, and monitor contractile responses to electrical stimuli (rectangular pulses, 2-ms duration for 3D constructs) using appropriate magnification. If construct is too large to observe on a standard microscope, use a stereomicroscope instead.
- (v) To assess electrical excitability, increase signal amplitude in 0.1 V increments up to 10 V, and the stimulation frequency up to 400 beats per minute.
- (vi) For each combination of voltage and frequency, look for the presence of random, spontaneous contractions (an indicator of immature tissue) versus synchronous contractions in response to electrical pacing (an indicator of more mature tissue containing electromechanically coupled cells).
- (vii) Measure excitation threshold (ET; the minimum voltage of electrical stimulation required to elicit sustained synchronous contractions of the whole tissue construct at a frequency of 60 beats per minute).
- (viii) Measure the maximum capture rate (MCR; maximum frequency of sustained synchronous contractions that can be achieved at a stimulation voltage corresponding to 1.5 ET).
- (ix) To assess the magnitude of contractions of engineered cardiac constructs visually, measure fractional area change of tissue in response to electrical field stimulation. Set up video camera and microscope magnification to allow construct to occupy as much of the captured frame as possible. If this is not possible because of the size of the construct, use a stereomicroscope instead. Adjust lighting for maximum contrast of scaffold versus background by placing a black object under the scaffold, and eliminating any reflective objects from view.
- (x) Record video of scaffold being paced at a frequency of 1 Hz and a stimulus of 1.5× ET for 3 s (with at least 30 frames per second), and save in AVI (audio video interleave) format.
- (xi) Perform video analysis (can be performed at a later time on saved movie files) by opening video using the custom MATLAB software (available in Supplementary Data 1 online; also see Supplementary Manual 1 online; screen capture shown in Fig. 5a). Our custom MATLAB software first opens each frame from the loaded movie file, converts the images to grayscale and then to binary with a threshold value that is set by the user, and depends on lighting conditions of movie recording. Finally, the area of the largest object in each image (which should correspond to that of the scaffold) is stored in a format that can be pasted into spreadsheet software (such as EXCEL).
- (xii) Drag the slider to set the appropriate image threshold and press 'Process video' button. As the video is processed, a figure in the top right-hand corner of the screen displays a trace of the calculated area.
- (xiii) When calculations are finished, paste data into spreadsheet software, select the maximum and minimum size of tissue during each contraction and perform the following calculation for fractional change of area: (relaxed size contracted size)/(relaxed size).

# (B) End-point analytics—cell alignment and elongation (for monolayer cultures only) • TIMING 90 min setup per staining + 2 h per sample

- (i) Perform live/dead stain on monolayer of cells from Step 20 and take both fluorescent and bright field images of the same area; for live/dead staining, incubate the cells in 0.7 ml (for one well of a 6-well dish, two coverslips or tables per well) of solution of carboxyfluorescein diacetate (10 μM) and PI (75 μg ml<sup>-1</sup>) in PBS for 60 min, followed by rinsing in PBS (two times) and imaging. Other fluorescent live/dead kits can also be used for this purpose.
- (ii) Open pair of images in ImageJ software (available at http://rsb.info.nih.gov/ij/).**CAUTION** The steps below rely on user input.
- (iii) Enlarge the images until the cell outlines (bright green) are clearly visible. Draw lines corresponding to the cell's long and short axes in the fluorescent image (**Fig. 5c**).
- (iv) For cells cultured on abraded surfaces, draw a line on the bright-field image corresponding to the direction of abrasions and measure the angle between the abrasion and the cell's long axis.
- (v) For cells cultured on nonabraded surfaces, you can measure the angle between the cell's long axis and either the axis that was orthogonal or parallel to the electrical field. In our past studies, for example, we have compared the angle of the long axis of fibroblasts to the orthogonal direction, and the angle for cardiomyocytes to the parallel direction. These directions were selected on the basis of the previous studies that have demonstrated that fibroblasts align orthogonal<sup>33</sup>, whereas cardiomyocytes align parallel to the electrical field lines<sup>8</sup> (see **Box 1** for a technique for aligning fibroblasts orthogonal to the electrical field within just 3 h).
- (vi) Determine elongation by measuring the long and short axes of the cell and calculating the aspect ratio (long-to-short axis ratio). Exclude from analysis any cells of which the perimeters cannot be precisely determined (this number should not be more than 10%). We measure a total of 60–90 cells per group from at least N = 3 independent experiments (e.g., 20–30 cells per sample).



**Figure 5** Methods for quantitative image analysis for Steps 21A, B and C. (a) Assessing magnitude of contractions for engineered cardiac tissue (Step 21A). A slider allows the user to select the image threshold and to see the calculated magnitude of the contractions on the screen or to export the data to spreadsheet software. (b) Connexin-43 analysis (Step 21C). A slider allows the user to select the image threshold and see the outlines of the identified gap junctions and cell nuclei. (c) Live-dead staining (left) and bright-field image (right) of the same field for assessment of cell elongation and alignment (Step 21B). Annotations (in yellow) correspond to a cell's long and short axes (in the live-dead image) and the corresponding surface's direction of abrasions (in the bright-field image). Scale bars correspond to 50 µm.

# (C) End-point analytics—histological analysis (including analysis of gap junctions) • TIMING 1-3+ d

- (i) Fix monolayers or 3D constructs from Step 20, 21A or 21B (monolayers, in 2% (vol/vol) formaline, 1 h; 3D constructs, in 10% formaline, 24 h).
- (ii) (3D constructs) Embed and section in paraffin blocks.
  - **!** CAUTION The processing, embedding and sectioning of paraffin blocks requires specialized equipment and expertise and is usually performed by a histology or pathology laboratory. Although hand processing can be performed by following several available protocols (e.g., http://www.ihcworld.com/\_protocols/histology/paraffin\_section.htm, http:// www.bdbiosciences.com/pharmingen/protocols/Paraffin\_Sections.shtml) the results may show marked variation in histology quality and antigenicity.

■ PAUSE POINT Sectioned slides may be stored at RT (18–24 °C) or at 4 °C indefinitely until required.

- (iii) (3D constructs) Deparafinize sections to retrieve antigen by heat treatment for 20 min at 95 °C in a decloaking chamber (Biocare Medical).
- (iv) Block sections with  $\sim$  200 µl (or enough to cover cells) of 10% horse serum diluted in PBS for 30 min at RT (18–24 °C) in a dark, humidified chamber.

**CRITICAL STEP** For Steps C(iv-xi), neonatal rat heart and bovine tendon can serve as positive and negative controls, respectively.

- (v) Incubate three times in 200  $\mu l$  of PBS for 5 min at RT (18–24  $^\circ C)$  in a dark, humidified chamber.
- (vi) Incubate the sections for 1 h at 37 °C with 200 μl of either TnI or Cx-43 (1:150 dilution for each antibody in PBS containing 0.5% (vol/vol) Tween 20 and 1.5% (vol/vol) horse serum).
- (vii) Incubate three times in 200  $\mu l$  of PBS for 5 min at 37  $^\circ C.$
- (viii) For TnI, incubate sections at RT for 30 min with 200 μl of the secondary antibody solution (horse anti-mouse IgG 1:200 dilution in PBS containing 0.5% (vol/vol) Tween 20 and 1.5% (vol/vol) horse serum); for Cx-43, use fluorescein-conjugated goat anti-rabbit IgG (1:200 dilution in PBS containing 0.5% (vol/vol) Tween 20 and 1.5% (vol/vol) horse serum).
- (ix) Incubate three times in 200  $\mu l$  of PBS for 5 min at 37  $^\circ C$  .

- (x) Apply one drop of DAPI mounting solution on top of the sample and cover with a coverslip.
- (xi) Assess construct architecture and cell distribution from the stained sections using fluorescent microscope (Axioplan, Zeiss). In particular, look at the positions of the cells relative to the scaffold pores, the depth of the cells relative to the edge of the scaffold and the orientation of the long axis of the cells.
- (xii) To perform gap junctional analysis (for samples stained for Cx-43), open the custom MATLAB software (available in Supplementary Data 2 online; also see Supplementary Manual 2 online; screen capture shown in Fig. 5b).
  ▲ CRITICAL STEP The algorithm for our custom MATLAB software first reads in an image file for Cx-43 staining (that the user inputs), estimates the background illumination, subtracts the background image from the original image, converts the corresponding image to gray scale intensity image and then converts the image to binary with a threshold value that is to be set by the user depending on lighting conditions. Finally, the number of objects in this processed binary image (excluding those objects outside the user-defined size-thresholds) are labeled and counted.

**CRITICAL STEP** For Steps C(xii–xvii), images will need to be collected through fluorescein isothiocyanate and DAPI filters separately.

- (xiii) Press 'Open Connexin Image' button (and select image of cells stained for fluorescently labeled Cx-43) and the image will appear in the top left-hand corner of the screen.
- (xiv) Drag the sliders to adjust the appropriate image threshold, minimum and maximum size (in pixels) of gap junctions to count, respectively. The resulting processed image will appear in the top right-hand corner of the screen.
- (xv) Repeat Steps C(xiii-xiv) for the corresponding DAPI image (and resulting image will appear in the bottom half of the screen).
- (xvi) Note the results for (i) the total number of gap junctions counted, (ii) total number of nuclei counted and (iii) the ratio of gap junctions/nuclei, which will all appear in a box in the bottom right-hand corner of the screen.
- (xvii) Repeat Steps 21 C(xiii-xvi) for all desired images to be analyzed.

# (D) End-point analytics—ultrastructure analysis • TIMING 2+ d

(i) Prepare either 3D constructs or monolayer samples from Step 20 for transmission electron microscopy (TEM), which allows observation of gap junction and z-band formation. Details of fixation, embedding and sectioning are described elsewhere<sup>34</sup>. In short, cells are fixed in Karnovsky's reagent (a mixture of sodium cacodylate, paraformaldehyde and gluteraldehyde), post-fixed in osmium tetroxide in veronal-acetate buffer, dehydrated in graded ethanol in propylene oxide, embedded in Epon 812 (Polysciences), cut into thin sections (70 nm) using a diamond knife and stained with lead citrate and uranyl acetate.

**!** CAUTION Because the processing of samples for TEM requires many flammable and toxic materials, you may prefer to have your samples prepared by a biological TEM laboratory for processing.

- (ii) Examine sections for ultrastructural properties relevant to cardiac tissue (volume fraction and developmental stage of sarcomeres, Z and M lines, H, I and A bands, gap junctions, T tubules) using a Philips EM410 transmission electron microscope operated at 80 kV (JEOL-100CX, JEOL).
- (iii) Perform morphometric analysis on 20–46 randomly taken transmission electron micrographs at a magnification of  $\times$ 100,000. A test grid with uniform squares (0.26 cm  $\times$  0.26 cm) is superimposed onto the micrographs and the areas covered by sarcomeres, mithochondria, nuclei and the overall area of the cells are determined. The volume fraction of each organelle is determined as described previously<sup>8</sup>. The frequency of intercalated disks and gap junctions (number per mm<sup>2</sup>) is determined by counting. A total of 20 micrographs of nonstimulated constructs, 46 micrographs of stimulated constructs and 42 micrographs of neonatal ventricles were evaluated with respect to each structural parameter by two independent observers.

# • TIMING

Steps 1-8: preparation of electrical stimulation chamber (30 min per chamber)

Step 9: sterilization of electrical stimulation chamber (40 min, 24 h before the experiment)

Step 10: cell preparation (12–18 h); option A (monolayers): prepare (microabraded or smooth) surface (27 h), cell seeding onto (microabraded or smooth) surface (3 h); option B (3D constructs): preparation of ultrafoam collagen scaffolds (3 h), scaffold seeding using Matrigel (30 min per 6 scaffolds)

Steps 11 and 12: assembling culture chamber (30 min)

Steps 13-20: applying and checking electrical stimulation (1 h)

Steps 14A and 14B: tissue culture (3-8 d)

Step 21: assessments—option A: contractile activity (3D constructs: 1 h + 10 min per scaffold); option B: cell alignment/ elongation (monolayers: 1.5 h + 2 h per sample); option C: histology (1-3+d); option D: ultrastructure (2+d)

# TROUBLESHOOTING

Troubleshooting advice can be found in Table 1.

**TABLE 1** | Troubleshooting table.

Step number and problem	Possible reason	Solution
Electrical stimulation		
Step 6: electrodes are not connected properly when checked with multimeter	Perhaps the wire is not wrapped tightly enough under the RTV adhesive	Wrap wire more tightly around the electrode; make sure that silicone adhesive is not between the electrode and the platinum wire
Step 12: trouble keeping scaffolds placed in culture chamber	Too much medium in culture chamber, or too much movement involved with placing chamber in incubator	Try placing pieces of autoclaved PDMS (poly dimethyl siloxane) blocks between scaffolds as spacers. These blocks will not interfere with the electric field stimulus
Step 14: during stimulation, culture medium becomes clear	Stimulation amplitude is too high for the amount of medium	Add more medium, or change medium more often
Steps 15 and 16: Trouble measuring current in bioreactor	Choose the appropriate value of the resistor $R_m$ in the circuit shown in <b>Figure 4a</b>	Remember that the value of the resistor should be small compared with that of the resistance of the bioreactor, but that it should still be large enough to measure a voltage across it
		It could also be that there is in fact an open circuit somewhere in the system, and so it is also wise to check the connections between all connected parts. A multimeter will help to check whether parts you have connected to each other are indeed connected
		There could also be a short circuit somewhere in your system if, for example, you are performing measurements on a metal surface or with unin- sulated wires
Step 17: the waveform applied to my cells appears smaller in amplitude than expected	Perhaps your stimulus generator has a current rating that is too low	Try reducing the amplitude of stimulation or shortening the electrodes, or consider buying a stimulator with a higher current rating or building an amplifier circuit to boost the power of your signal (see <b>Box 3</b> ). It could also be that you have too many stimulation chambers connected in parallel
Microabrasions		
Step 10A: abrasions are not straight enough	Lapping not done in a consistent direction	Try lapping only in a single direction (not lapping back and forth, but lapping each stroke separately)
Contamination		
Step 14: culture is contaminated	Changing medium	Be careful when changing medium not to allow any medium to splash onto the lid of the culture chamber. Placing the culture chamber on top of a 150-mm Petri dish can facilitate carry- ing and placing the electrical setup within the incubator. In addition, wearing sterile gloves whenever handling the bioreactor during cell culture can help
	Sterilization procedures	Autoclave in sterilization pouches (not in alu- minum foil or paper)

# ANTICIPATED RESULTS

We have found in our previous studies that electrical stimulation utilized during cultivation of cardiac cell populations and 3D engineered tissues has been critical for the maintenance of differentiated cell phenotype and cell assembly into synchronously contractile cardiac tissues. We summarize here the effects of electrical stimulation for two representative situations: electrical stimulation of (i) cardiac cells cultured in monolayer (on both abraded and unabraded polyvinyl substrates) and (ii) 3D engineered cardiac tissue constructs.

## Effects of electrical field stimulation and substrate topography on monolayer-cultured fibroblasts and cardiomyocytes

When we abrade the polyvinyl surfaces as described in this protocol, we see peak-to-peak distances of 13  $\mu$ m between grooves and a depth of 700 nm (**Fig. 3**). When we cultured cardiac myocytes in monolayer on these surfaces, after the application of electrical field stimulation (Steps 13 and 14) of amplitudes of 2.3 or 4.6 V/cm, either parallel or orthogonal to the direction of abrasions (with nonabraded surfaces used as controls), we observed that cells (in all cases) elongated and aligned with their axis parallel to the surface abrasions (**Fig. 6**). This abrasion type gave us the highest degree of alignment and elongation, consistent with previously reported studies that utilized grooves of precisely defined dimensions<sup>35–37</sup> as well as the rough surfaces<sup>38</sup>. As the abrasions were oriented either (i) parallel to the electrical field (i.e., orthogonal to the electrodes) or (ii) orthogonal to the electrical field (i.e., parallel to the electrodes), the two cues (topography and electrical field) acted on the cells either in a parallel or in an orthogonal direction (**Fig. 3c**). In the first case, the electrical field and topography were acting on the cell alignment in the same direction. In the second case, the field was acting on the cell in the orthogonal direction to the abrasions. On unabraded monolayer surfaces, pulsatile electrical field significantly enhanced elongation of cardiomyocytes (**Fig. 6a**) to reach the levels comparable with that achieved by surface abrasion.

The fact that field stimulation failed to promote elongation at higher levels than that obtained by topographical cues prompted us to hypothesize that the pathway for elongation is saturated by topographical cues, and that the same signaling pathways could be involved in the cellular response (i.e., elongation) to topographical cues and electrical field stimulation. In addition, pulsatile electrical field stimulation significantly enhanced orientation of cardiomyocytes (**Fig. 6b**) when they were cultivated on abrasions placed orthogonal to the field lines. Yet, within every voltage group, the nonabraded surfaces had approximately two times higher average orientation angle than the abraded surfaces (**Fig. 6b**), indicating that topographical cues are overall a stronger regulator of cellular orientation than field stimulation.

Phalloidin–TRITC staining indicated that actin filaments generally followed the direction of surface abrasions<sup>22</sup>. For cells cultivated on nonabraded surfaces, actin cytoskeleton was disorganized. Higher magnification images (**Fig. 6c**) revealed remarkable differences in orientation of actin filaments as a function of surface abrasion and electrical field stimulation. On abraded surfaces, actin filaments were clearly aligned in the direction of surface abrasions (either orthogonal or parallel to the field lines). For cardiomyocytes cultivated on nonabraded surfaces at 0.0 and 2.3 V/cm (**Fig. 6c**), the actin cytoskeleton was not

aligned in any particular direction, and the overlapping filaments were extending in multiple directions. Yet, at 4.6 V/cm on nonabraded surfaces (**Fig. 6c**), there was an appreciable improvement in the organization of the actin filaments, which aligned in parallel along the long axis of the cell.

As we saw similar results with 3T3 fibroblasts and, furthermore, observed

**Figure 6** | Cardiomyocytes cultivated on abraded and nonabraded surfaces in the presence of electrical field stimulation. The surfaces were obtained using lapping paper with a grain size of 80 μm. Electrical field stimulation using square pulses 1-ms duration, 1 Hz and 2.3 or 4.6 V/cm was initiated 24 h after cell seeding and maintained for additional 72 h. (a) Cell elongation as defined by the aspect ratio and (**b**) cell orientation as measured by the angle between the abrasion and the long axis of the cell. In a and b: light gray bars: abrasions oriented orthogonal to the electrical field; dark gray bars: abrasions oriented parallel to the electrical field; and white bars: nonabraded surfaces. Data are represented as averages  $\pm$  s.d. Total N = 2-3 independent samples (coverslips) per group; 30-90 cells were analyzed per group (P < 0.05 was considered significant). \*Significantly different than nonabraded surface at identical stimulation voltage. (c) Actin cytoskeleton as visualized by phalloidin-TRITC staining (scale bar is 10 µm, electrical field lines are from left to right). Yellow lines indicate the directionality of the surface abrasions.

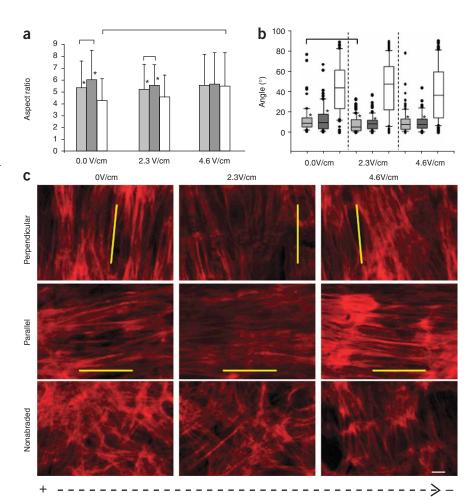
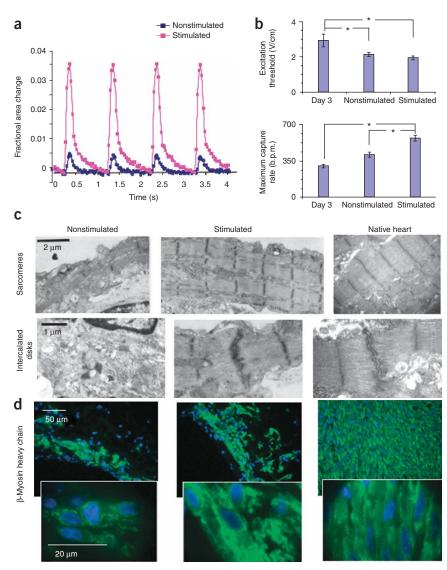


Figure 7 | Orderly excitation-contraction coupling enhances functional assembly of myocardium in vitro. (a) Contraction amplitude (the fractional change in area of tissue during a contraction) increases with electrical stimulation. (b) Excitation threshold (electrical field voltage gradient that needs to be applied to induce synchronous contractions of cultured tissue constructs) and maximum capture rate (the maximum frequency at which tissue constructs can be induced to beat) significantly decreased and increased, respectively, with the application of electrical stimulation and with time in culture. (c) Ultrastructural organization. Representative transmission electron micrographs of stimulated and nonstimulated constructs after 8 d of cultivation, compared with neonatal rat ventricles are shown (top: structure of a sarcomere; bottom: intercalated disk). Electrical stimulation induced the development of long, well-aligned registers of sarcomeres, and in stimulated constructs, intercalated disks were positioned between aligned Z lines and were as frequent as in neonatal ventricles. (d)  $\beta$ -Myosin heavy chain staining. Stimulated constructs and neonatal ventricles contained higher levels compared with unstimulated constructs.

the abolishment of the orientation and elongation response of cardiomyocytes to the abraded surfaces and electrical field stimulation by inhibition of actin polymerization (and only partially by inhibition of PI3K pathway), we conclude that the surface topography more strongly determined the orientation of both fibroblasts and cardiomyocytes than pulsatile electrical field<sup>22</sup>. These findings have implications for the



design of scaffolds for cardiac tissue engineering. A feasible strategy would be to design scaffolds of desired microarchitecture (e.g., by electrospinning) to drive cellular elongation and orientation in the desired direction, followed by the application of electrical field stimulation for enhancement of these properties.

# Electrical stimulation of engineered cardiac tissue

In native heart, electrical signals generated by pacing cells spread throughout the heart and cause the depolarization of cellular membranes and activation of the contractile apparatus in cardiac myocytes<sup>39</sup>. The application of electrical stimulation to cardiac constructs markedly enhanced the contractile behavior. After 8 d of culture, the amplitude of contractions was sevenfold higher in stimulated than in nonstimulated constructs (**Fig. 7a**), a result of the progressive increase with the duration of culture.

Although the ET (the minimum voltage at which the entire construct was observed to beat) for stimulated constructs was not significantly smaller than the one for nonstimulated constructs at 8 d of culture, the MCR (the maximum rate the entire construct could be paced) was significantly higher in the stimulated group compared with the nonstimulated group at 8 d of culture (**Fig. 7b**). The shape, amplitude ( $\sim$  100 mV) and duration ( $\sim$  200 ms) of the electrical activity recorded for cells in constructs stimulated during culture were similar to action potentials reported for constructs that were mechanically stimulated during culture<sup>7</sup>.

Engineered constructs that were electrically stimulated during culture demonstrate a remarkable level of ultrastructural differentiation, comparable in several respects with that of native myocardium (**Fig. 7c**). Myofibers align orthogonal to the direction of the electrodes, within the top  $\sim 200 \,\mu\text{m}$  of the construct thickness. The collagen sponge scaffold consists of isotropic interconnected pores 190  $\mu\text{m}$  in diameter<sup>40</sup>, but as the sponge is biodegradable, the seeded cells can remodel the matrix during the alignment process, possibly in an attempt to decrease the apparent ET in response to pacing<sup>41</sup>. In contrast,

# cells in nonstimulated constructs stayed round and expressed relatively low levels of cardiac markers. Electrical stimulation also increased the amounts of mitochondria and glycogen, and induced the formation of well-aligned registers of sarcomeres that closely resembled those in native myocardium (**Fig. 7c**), representing a hallmark of maturing cardiomyocytes<sup>39</sup>. The volume fraction of sarcomeres in stimulated 8-d constructs was indistinguishable from that measured for neonatal ventricles<sup>42</sup>, in contrast to nonstimulated constructs with only scarce and poorly organized sarcomeres. Stimulated constructs also had well-developed intercalated disks and gap junctions. Electrical stimulation also elevated the levels of $\beta$ -MHC (**Fig. 7d**), Cx-43, creatine kinase-MM and cardiac Tn-I<sup>8</sup>.

Note: Supplementary information is available via the HTML version of this article.

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- Mitcheson, J.S., Hancox, J.C. & Levi, A.J. Cultured adult cardiac myocytes: future applications, culture methods, morphological and electrophysiological properties. *Cardiovasc. Res.* 39, 280–300 (1998).
- Carrier, R. et al. Perfusion improves tissue architecture of engineered cardiac muscle. *Tissue Eng.* 8, 175–188 (2002).
- Ellingsen, O. et al. Adult rat ventricular myocytes cultured in defined medium: phenotype and electromechanical function. Am. J. Physiol. Heart Circ. Physiol. 265, H747–H754 (1993).
- Volz, A., Piper, H.M., Siegmund, B. & Schwartz, P. Longevity of adult ventricular rat heart muscle cells in serum-free primary culture. J. Mol. Cell. Cardiol. 23, 161–173 (1991).
- Radisic, M. et al. Medium perfusion enables engineering of compact and contractile cardiac tissue. Am. J. Physiol. Heart Circ. Physiol. 286, H507–H516 (2004).
- Radisic, M. *et al.* Biomimetic approach to cardiac tissue engineering: oxygen carriers and channeled scaffolds. *Tissue Eng.* 12, 2077–2091 (2006).
- Zimmermann, W.H. et al. Tissue engineering of a differentiated cardiac muscle construct. Circ. Res. 90, 223 (2002).
- Radisic, M. *et al.* From the cover: functional assembly of engineered myocardium by electrical stimulation of cardiac myocytes cultured on scaffolds. *PNAS* **101**, 18129–18134 (2004).
- Feng, Z., Matsumoto, T., Nomura, Y. & Nakamura, T. An electro-tensile bioreactor for 3-D culturing of cardiomyocytes. *IEEE Eng. Med. Biol. Mag.* 24, 73–79 (2005).
- Radisic, M. et al. Biomimetic approach to cardiac tissue engineering. Philos. Trans. R. Soc. Lond. B Biol. Sci. 362, 1357–1368 (2007).
- Hart, R.A. & Gandhi, O.P. Comparison of cardiac-induced endogenous fields and power frequency induced exogenous fields in an anatomical model of the human body. *Phys. Med. Biol.* 43, 3083–3099 (1998).
- 12. Bian, W. & Tung, L. Structure-related initiation of reentry by rapid pacing in monolayers of cardiac cells. *Circ. Res.* **98**, e29–e38 (2006).
- Kong, C.-R., Bursac, N. & Tung, L. Mechanoelectrical excitation by fluid jets in monolayers of cultured cardiac myocytes. J. Appl. Physiol. 98, 2328–2336 (2005).
- Sathaye, A., Bursac, N., Sheehy, S. & Tung, L. Electrical pacing counteracts intrinsic shortening of action potential duration of neonatal rat ventricular cells in culture. J. Mol. Cell. Cardiol. 41, 633–641 (2006).
- Berger, H.J. *et al.* Continual electric field stimulation preserves contractile function of adult ventricular myocytes in primary culture. *Am. J. Physiol. Heart Circ. Physiol.* 266, H341–H349 (1994).
- Levin, M. Motor protein control of ion flux is an early step in embryonic left-right asymmetry. *BioEssays* 25, 1002–1010 (2003).
- Feld, Y. *et al.* Electrophysiological modulation of cardiomyocytic tissue by transfected fibroblasts expressing potassium channels: a novel strategy to manipulate excitability. *Circulation* **105**, 522–529 (2002).
- Munoz, V. *et al.* Adenoviral expression of IKs contributes to wavebreak and fibrillatory conduction in neonatal rat ventricular cardiomyocyte monolayers. *Circ. Res.* **101**, 475–483 (2007).
- 19. Nuccitelli, R. Endogenous ionic currents and DC electric fields in multicellular animal tissues. *Bioelectromagnetics*. (Suppl 1): 147–157 (1992).
- Ypey, D.L., Clapham, D.E. & DeHaan, R.L. Development of electrical coupling and action potential synchrony between paired aggregates of embryonic heart cells. *J. Membrane Biol.* **51**, 75–96 (1979).
- Tandon, N., Cannizzaro, C., Figallo, E., Voldman, J. & Vunjak-Novakovic, G. Characterization of electrical stimulation electrodes for cardiac tissue engineering. *Conf. Proc. IEEE Eng. Med. Biol. Soc.* 1, 845–848 (2006).

 Au, H.T., Cheng, I., Chowdhury, M.F. & Radisic, M. Interactive effects of surface topography and pulsatile electrical field stimulation on orientation and elongation of fibroblasts and cardiomyocytes. *Biomaterials* 28, 4277–4293 (2007).

PROTOCOL

- Park, H. et al. Electrical stimulation and extracellular matrix remodeling of C2C12 cells cultured on collagen scaffolds. J. Tissue Eng. Regen. Med. 2, 279–287 (2008).
- 24. Chao, P.H. *et al.* Chondrocyte translocation response to direct current electric fields. *J. Biomech. Eng.* **122**, 261–267 (2000).
- Reid, B., Nuccitelli, R. & Zhao, M. Non-invasive measurement of bioelectric currents with a vibrating probe. *Nat. Protoc.* 2, 661–669 (2007).
- Song, B. *et al.* Application of direct current electric fields to cells and tissues *in vitro* and modulation of wound electric field *in vivo*. *Nat. Protoc.* 2, 1479–1489 (2007).
- Radisic, M., Marsano, A., Maidhof, R., Wang, Y. & Vunjak-Novakovic, G. Cardiac tissue engineering using perfusion bioreactor systems. *Nat. Protoc.* 3, 719–738 (2008).
- Tandon, N., Marsano, A., Cannizzaro, C., Voldman, J. & Vunjak-Novakovic, G. Design of electrical stimulation bioreactors for cardiac tissue engineering. *Conf. Proc. IEEE Eng. Med. Biol. Soc.* 1, 3594–3597 (2008).
- Durand, D. Electric stimulation of excitable tissue. In *The Biomedical Engineering* Handbook (eds. Durand, D., & Bronzino, J.D.), 229–251 (CRC Press, Boca Raton, FL, 1995).
- Cannizzaro, C. et al. Practical aspects of cardiac tissue engineering with electrical stimulation. Methods. Mol. Med. 140, 291–307 (2007).
- Loe, M.J. & Edwards, W.D. A light-hearted look at a lion-hearted organ (or, a perspective from three standard deviations beyond the norm) Part 1 (of two parts). *Cardiovasc. Pathol.* 13, 282–292 (2004).
- Norlin, A., Pan, J. & Leygraf, C. Investigation of electrochemical behavior of stimulation/sensing materials for pacemaker electrode applications. J. Electrochem. Soc. 152, J7–J15 (2005).
- Erickson, C.A. & Nuccitelli, R. Embryonic fibroblast motility and orientation can be influenced by physiological electric fields. J. Cell Biol. 98, 296–307 (1984).
- Graham, L. & Orenstein, J.M. Processing tissue and cells for transmission electron microscopy in diagnostic pathology and research. *Nat. Protoc.* 2, 2439–2450 (2007).
- Flemming, R.G., Murphy, C.J., Abrams, G.A., Goodman, S.L. & Nealey, P.F. Effects of synthetic micro- and nano-structured surfaces on cell behavior. *Biomaterials* 20, 573–588 (1999).
- Clark, P., Connolly, P., Curtis, A.S., Dow, J.A. & Wilkinson, C.D. Cell guidance by ultrafine topography *in vitro*. J. Cell Sci. 99, 73–77 (1991).
- Clark, P., Connolly, P., Curtis, A.S., Dow, J.A. & Wilkinson, C.D. Topographical control of cell behaviour: II. Multiple grooved substrata. *Development* 108, 635–644 (1990).
- Eisenbarth, E., Meyle, J., Nachtigall, W. & Breme, J. Influence of the surface structure of titanium materials on the adhesion of fibroblasts. *Biomaterials* 17, 1399–1403 (1996).
- 39. Severs, N.J. The cardiac muscle cell. BioEssays 22, 188-199 (2000).
- Shen, Y.H., Shoichet, M.S. & Radisic, M. Vascular endothelial growth factor immobilized in collagen scaffold promotes penetration and proliferation of endothelial cells. *Acta Biomaterialia* 4, 477–489 (2008).
- Bursac, N., Parker, K.K., Iravanian, S. & Tung, L. Cardiomyocyte cultures with controlled macroscopic anisotropy: a model for functional electrophysiological studies of cardiac muscle. *Circ. Res.* **91**, e45–e54 (2002).
- Olivetti, G., Anversa, P. & Loud, A.V. Morphometric study of early postnatal development in the left and right ventricular myocardium of the rat. II. Tissue composition, capillary growth, and sarcoplasmic alterations. *Circ. Res.* 46, 503–512 (1980).
- Soong, H., Parkinson, W., Sulik, G. & Bafna, S. Effects of electric fields on cytoskeleton of corneal stromal fibroblasts. *Curr. Eye Res.* 9, 893–901 (1990).
   Frickson, C.A. Control of nound crest call dispersion in the truck of the axia.
- Erickson, C.A. Control of neural crest cell dispersion in the trunk of the avian embryo. *Dev. Biol.* 11, 138–157 (1985).
   Eviction of Mathematical Control of Con
- Nishimura, K.Y., Isseroff, R.R. & Nuccitelli, R. Human keratinocytes migrate to the negative pole in direct current electric fields comparable to those measured in mammalian wounds. J. Cell Sci. 109, 199–207 (1996).