

# 1 **Cu<sub>2</sub>O-based catalysts for the electrochemical reduction of** 2 **CO<sub>2</sub> at gas-diffusion electrodes**

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9

## 10 **Abstract**

11 Gas-diffusion electrodes are prepared with commercial Cu<sub>2</sub>O and Cu<sub>2</sub>O-ZnO mixtures  
12 deposited onto carbon papers and evaluated for the continuous CO<sub>2</sub> gas phase  
13 electroreduction in a filter-press electrochemical cell. The process mainly produced  
14 methanol, as well as ethanol and n-propanol. The analysis includes the evaluation of key  
15 variables with effect in the electroreduction process: current density ( $j= 10$  to  $40$   
16  $\text{mA}\cdot\text{cm}^{-2}$ ), electrolyte flow/area ratio ( $Q_e/A= 1$  to  $3 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ ) and CO<sub>2</sub> gas  
17 flow/area ratio ( $Q_g/A= 10$  to  $40 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ ), using a  $0.5 \text{ M KHCO}_3$  aqueous solution.

18 The maximum CO<sub>2</sub> conversion efficiency to liquid-phase products was 54.8% and  
19 31.4% for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, at an applied potential of  $-1.39$  and  $-$   
20  $1.16 \text{ V}$  vs. Ag/AgCl, respectively. Besides, the Cu<sub>2</sub>O/ZnO electrodes are expected to  
21 catalyse the CO<sub>2</sub> electroreduction for over 20 h. These results may provide new insights  
22 into the development of powerful electrocatalysts for reduction of CO<sub>2</sub> in gas phase to  
23 alcohols.

24 **Keywords:** Electrochemical reduction, carbon dioxide, gas-diffusion electrode, copper  
25 oxide, methanol

## 26 **1. Introduction**

27 Carbon dioxide (CO<sub>2</sub>) concentration in the atmosphere is increasing each year by about  
28  $2 \text{ mg}\cdot\text{l}^{-1}$ , continuing the inexorable rise toward  $400 \text{ mg}\cdot\text{l}^{-1}$  and beyond [1]. These high  
29 atmospheric CO<sub>2</sub> concentrations have been now widely accepted to produce severe  
30 environmental problems such as climate change. In the 21<sup>st</sup> century our world is still

31 searching for strategies to overcome the challenges associated with the climate change,  
32 as well as the dependency on fossil fuels and limited natural resources.

33 A variety of technologies to reduce CO<sub>2</sub> emissions have been applied through different  
34 methods. Currently, carbon capture and storage (CCS) has received considerable  
35 attention as one of the technologies to handle large quantities of CO<sub>2</sub> emissions [2],  
36 where CO<sub>2</sub> capture seems to be the bottleneck step where the efforts have to be applied  
37 [3-5]. Sequestration has been the major storage option for CO<sub>2</sub> gas from power plants,  
38 but several shortcomings remain, including environmental and safety concerns about the  
39 risk of leakage and technological limitations. Thus, new approaches to mitigate carbon  
40 output from the use of fossil fuels, as well as methods to fully exploit carbon neutral  
41 renewable energy sources are needed. A possible approach to slow down the increase in  
42 atmospheric CO<sub>2</sub> levels is the application of electrochemical methods in a Carbon  
43 Capture and Utilization (CCU) approach [6]. This technology is green and efficient and  
44 has aroused intense attention recently. The electrochemical reduction of CO<sub>2</sub> can not  
45 only offer a viable route to reuse CO<sub>2</sub>, but also a way to produce a number of valuable  
46 products, such as carbon monoxide (CO), formic acid (HCOOH), formaldehyde  
47 (CH<sub>2</sub>O), methanol (CH<sub>3</sub>OH), methane (CH<sub>4</sub>), ethanol (C<sub>2</sub>H<sub>6</sub>O), ethylene (C<sub>2</sub>H<sub>4</sub>) or n-  
48 propanol (C<sub>3</sub>H<sub>8</sub>O) [7-9]. Particularly, the challenges for converting CO<sub>2</sub> into CH<sub>3</sub>OH  
49 are great, but the potential rewards are also enormous [7, 10].

50 Currently, most electrodes used in the electroreduction of CO<sub>2</sub> are in the form of metal  
51 plates, metal granules or electrodeposited metals on a substrate [8]. However, owing to  
52 the relatively low solubility of CO<sub>2</sub> in water under ambient conditions, the reaction rates  
53 and current densities of CO<sub>2</sub> electroreduction are limited by the mass transfer of CO<sub>2</sub>  
54 from the bulk to the solid electrode surface [11, 12]. To improve the reduction process,  
55 gas diffusion electrodes (GDEs) have been proposed to alleviate mass transport  
56 limitations across the gas-liquid interface and to the catalyst surface [13-16]. A GDE is  
57 a porous composite electrode usually composed of polymer bonded catalyst particles  
58 and a carbon support. GDEs can be operated at higher current densities (200-600  
59 mA·cm<sup>-2</sup>). Besides, because of their high porosity and partial hydrophobicity, GDEs  
60 form a characteristic gas-solid-liquid three-phase interface, which allows a  
61 homogeneous distribution over the catalyst surface. These properties make GDEs  
62 especially suitable for CO<sub>2</sub> electroreduction in gas phase.

63 While significant research efforts have focused on the development of new catalyst  
64 materials, considerably fewer efforts have focused on the study of these catalysts after  
65 immobilization in GDEs. In the same manner, the literature on the application of GDEs  
66 for the electrochemical transformation of CO<sub>2</sub> to CH<sub>3</sub>OH is scarce [17-20]. Schwartz et  
67 al. [17] firstly studied perovskite-type crystal structures (A<sub>1.8</sub>A'<sub>0.2</sub>CuO<sub>4</sub>, A = La, Pr and  
68 Gd; A' = Sr and Th) in GDE for the electrochemical reduction of CO<sub>2</sub> under ambient  
69 conditions. The results showed that perovskite-type electrocatalysts could achieve  
70 cumulative Faradaic efficiencies for CO<sub>2</sub> reduction to CH<sub>3</sub>OH, C<sub>2</sub>H<sub>6</sub>O, and C<sub>3</sub>H<sub>8</sub>O up to  
71 40% at current densities of 180 mA·cm<sup>-2</sup>. In 2012, Aeshala et al. [18] developed Cu<sub>2</sub>O-  
72 based GDEs by electroplating the metal particles onto a carbon paper. These materials  
73 were settled in a reactor with different solid polymer electrolytes (i.e. SPEEK, Nafion,  
74 PVA, Amberlist) for continuous gas phase CO<sub>2</sub> electroreduction. The maximum  
75 Faradaic efficiencies were 0.54, 0.42, 0.3, and 4.5 for CH<sub>3</sub>OH, HCHO, CO and CH<sub>4</sub>  
76 production, respectively. The same group reported in 2013 a Faradaic efficiency as high  
77 as 45%, at a current density of 5.4 mA·cm<sup>-2</sup>, when applying an anionic solid polymer  
78 electrolyte membrane, with CH<sub>3</sub>OH as the main liquid product, and CH<sub>4</sub> and C<sub>2</sub>H<sub>4</sub> as  
79 major gaseous products. They concluded that the quaternary ammonium group in the  
80 solid polymer membrane, as well as the alleviated mass transfer limitation of CO<sub>2</sub> might  
81 have increase the efficiency of the GDE system [19]. Recently Lan et al. [20]  
82 investigated the electrochemical reduction of CO<sub>2</sub> on a Cu(core)/CuO(shell) catalyst in  
83 a flow reactor. This catalyst predominantly produce CO and HCOOH at 54.6 mA·cm<sup>-2</sup>,  
84 with a Faradaic efficiency of 21.5% and 20.2%, respectively. However, a small amount  
85 of CH<sub>3</sub>OH was also produced in the process (~2.5% Faradaic efficiency).

86 Furthermore, the literature demonstrated the good stability and notable catalytic ability  
87 of Cu<sub>2</sub>O-based surfaces for electrochemical hydrocarbons and/or alcohols formation  
88 from CO<sub>2</sub> [8, 11, 17-25]. Besides, the inclusion of ZnO may be the key for maintaining  
89 catalytic activity, since ZnO strengthen the Cu-CO<sup>-</sup> link, increasing the selectivity to  
90 alcohols, and stabilizing Cu in the hydrogenation reaction [11, 26-29]. Therefore, the  
91 primary objective of this study is to evaluate the performance of GDEs with spray  
92 supported Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO catalysts for the continuous electroreduction of CO<sub>2</sub> in  
93 gas phase. Then, an evaluation of the influence of key variables on the CO<sub>2</sub>  
94 electroreduction process (i.e. current density, electrolyte flow and CO<sub>2</sub> gas flow) is  
95 performed. The results are compared to those obtained in our previous work, where

96 mass transfer limitations were detected in the electroreduction of CO<sub>2</sub> in liquid phase  
97 when using a filter-press electrochemical cell.

98 The efforts carried out in this work will help to achieve the scale-up of CO<sub>2</sub> valorisation  
99 processes and devices in continuous operation, enabling a shift to a sustainable energy  
100 economy and chemical industry.

## 101 **2. Materials and methods**

### 102 *2.1. Preparation and characterization of the gas-diffusion electrodes*

103 The procedure to prepare the Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO GDEs has been described in detail  
104 previously [11]. The Cu<sub>2</sub>O-GDEs contain 1 mg·cm<sup>-2</sup> of metal particles. The catalyst  
105 loading was kept at 1 mg·cm<sup>-2</sup> of Cu<sub>2</sub>O and 1 mg·cm<sup>-2</sup> of ZnO for the Cu<sub>2</sub>O/ZnO  
106 electrodes. Briefly the procedure is as follows; Cu<sub>2</sub>O (Sigma Aldrich, particle size <  
107 5 μm, 97% purity) and ZnO particles (ACROS organic, < 45 μm, 99.5%) were mixed  
108 with a Nafion<sup>®</sup> dispersion 5 wt.% (Alfa Aesar) and isopropanol (IPA) (Sigma Aldrich),  
109 with a 70/30 catalyst/Nafion mass ratio and a 3% solids (catalyst + Nafion). This ink  
110 was airbrushed onto a porous carbon paper (TGP-H-60, Toray Inc.) and dried to get the  
111 electrodes. All electrodes were dried and rinsed with deionised water before use.

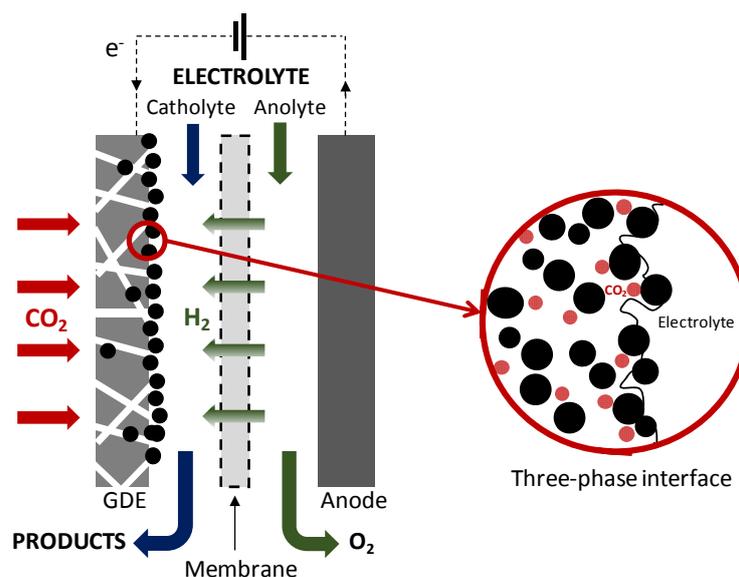
112 The EDX spectra and surface mapping confirmed the composition and uniform  
113 distribution of Cu<sub>2</sub>O-ZnO metal particles onto the carbon paper (See Figure A in  
114 Supporting Information). Thus, it can be inferred that the dispersion of the particles by  
115 air-brushing minimizes the agglomeration of the particles, which may greatly affect the  
116 electrode performance [23, 24, 29]. Besides the SEM cross-section image of the GDE  
117 shows that the diffusion layer (carbon paper) and the catalytic layer (Cu<sub>2</sub>O-ZnO)  
118 combined with each other tightly and the metallic particles covered nearly the entire  
119 carbon fibers of the support (See Figure B in Supporting Information).

### 120 *2.2. Electrochemical cell and experimental conditions*

121 The components of the experimental setup have been described in detail elsewhere [13].  
122 The electroreduction of CO<sub>2</sub> was carried out at ambient conditions using a filter-press  
123 electrochemical cell (Micro Flow Cell, ElectroCell A/S) in continuous operation. The  
124 cell was divided in a catholyte and anolyte compartments by a Nafion 117 cation  
125 exchange membrane. The membrane was treated prior the use following standard

126 procedures [30]. The airbrushed  $\text{Cu}_2\text{O}$  and  $\text{Cu}_2\text{O}/\text{ZnO}$ -catalysed papers were employed  
127 as the working electrodes (geometric area,  $A= 10 \text{ cm}^2$ ), together with a platinised  
128 titanium plate used as the counter electrode and a  $\text{Ag}/\text{AgCl}$  (sat.  $\text{KCl}$ ) reference  
129 electrode.

130 The cathode side of the reactor was fed with  $\text{CO}_2$  gas (99.99%) with a flow/area ratio  
131 ranging from  $10$  to  $40 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ , adjusted by a rotameter. A  $0.5 \text{ M KHCO}_3$   
132 (Panreac) aqueous solution is used as both, catholyte and anolyte, with a flow rate  
133 ranging from  $1$  to  $3 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ . The electrolytes were pumped from catholyte and  
134 anolyte tanks to the cell by two peristaltic pumps (Watson Marlow 320, Watson Marlow  
135 Pumps Group). In this study, the filter-press electrochemical system possesses three  
136 inputs (catholyte, anolyte and  $\text{CO}_2$  separately) and two outputs (catholyte- $\text{CO}_2$  and  
137 anolyte) for the electroreduction of  $\text{CO}_2$  in gas phase. Figure 1 schematically represents  
138 the electrolytic GDE cell configuration for the electroreduction of  $\text{CO}_2$  supplied directly  
139 from the gas phase.



**Fig. 1.** Schematic diagram of the electrolytic cell configuration for the electroreduction of  $\text{CO}_2$  supplied directly from the gas phase

140

141 The experiments were performed at galvanostatic conditions (i.e. at a constant current  
142 density), using an AutoLab PGSTAT 302N potentiostat (Metrohm, Autolab B.V.). The  
143 current density ranged from  $j= 5$  to  $40 \text{ mA}\cdot\text{cm}^{-2}$  in the electrochemical experiments.  
144 Liquid samples were taken every 15 minutes from the catholyte tank with a total

145 operational time of 90 minutes, where pseudo-stable values are obtained [11]. All the  
146 experiments were carried out at ambient conditions.

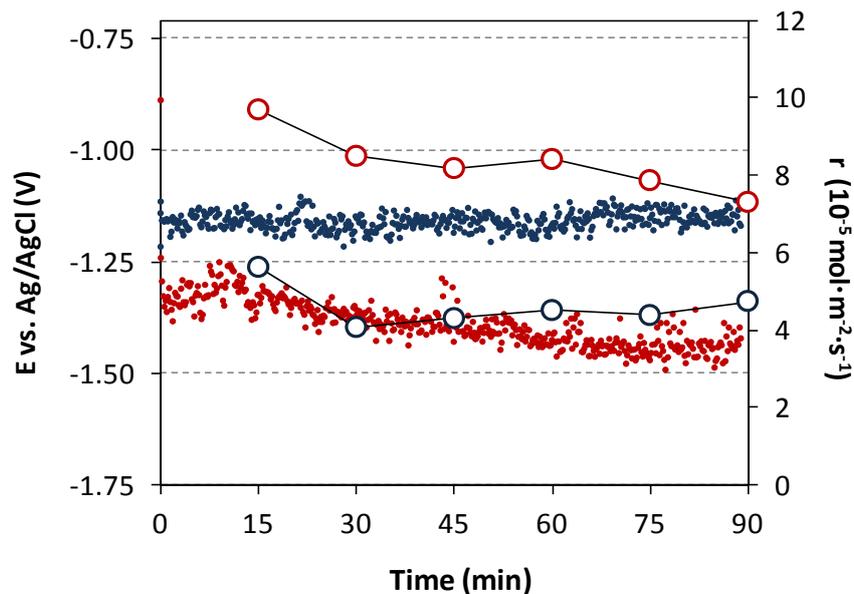
147 To quantify the concentration of each product in the liquid phase, the samples were  
148 analysed by duplicate in a headspace gas chromatograph (GCMS-QP2010, Ultra  
149 Shimadzu) equipped with a flame ionization detector (FID). Compounds were separated  
150 on a DB-Wax 30 m x 0.25 mm x 0.25  $\mu\text{m}$  column, with an injection and detector  
151 temperature of 250  $^{\circ}\text{C}$  and 270  $^{\circ}\text{C}$ , respectively. Helium was used as a carrier gas at a  
152 flow rate of 50  $\text{ml}\cdot\text{min}^{-1}$ . The identification of obtained products was further confirmed  
153 by headspace gas chromatography-mass spectrometry (GCMS-N5975B) using a 60 m x  
154 250  $\mu\text{m}$  x 1.40  $\mu\text{m}$  DB-624 capillary column. Three replicates were performed for each  
155 sample to obtain an averaged concentration of the formed products. The standard  
156 deviations of all the experiments were below 18.6 %.

157 The performance of the electrochemical process is evaluated by the rate of product  
158 formation,  $r$  (i.e. product obtained per unit of cathode area and time), and the Faradaic  
159 efficiency,  $FE$  (i.e. selectivity of the reaction for the production of each product). The  
160  $FE$  represents the percentage of the total charge supplied to the system that is used to  
161 form the different products.

### 162 **3. Results and discussion**

#### 163 *3.1. Continuous electroreduction of $\text{CO}_2$ in a filter-press electrochemical cell*

164 The electroreduction of  $\text{CO}_2$  at the  $\text{Cu}_2\text{O}$ -based GDEs led predominantly to the  
165 formation of  $\text{CH}_3\text{OH}$ , in accordance to those previous results at copper oxides surfaces  
166 [11, 24, 25]. Additionally, small quantities of  $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_3\text{H}_8\text{O}$  were also detected.  
167 Figure 2 shows the course of the applied voltage,  $E$ , and formation rate,  $r$ , of the main  
168 liquid-phase product,  $\text{CH}_3\text{OH}$ , over time for the  $\text{CO}_2$  electroreduction at both electrodes  
169 at ambient conditions.



**Fig. 2.** Electrocatalytic activity for the conversion of CO<sub>2</sub> at Cu<sub>2</sub>O (in red) and Cu<sub>2</sub>O/ZnO (in blue) GDEs. The figure shows the applied voltage,  $E$ , for a constant current of  $j=10\text{mA}\cdot\text{cm}^{-2}$  and the averaged rate of CH<sub>3</sub>OH formation,  $r$ , with time.

170

171 From the figure, the required voltage,  $E$ , remains stable for the Cu<sub>2</sub>O/ZnO-based  
 172 electrodes over the course of the 90 minutes of operation. In contrast, the Cu<sub>2</sub>O  
 173 electrode required an increasing applied voltage to maintain a stable current ( $j=10$   
 174  $\text{mA}\cdot\text{cm}^{-2}$ ), which may be related to the progressive detachment of catalyst particles  
 175 from the GDE surface and the deactivation due to the exposure to concentrated CO<sub>2</sub> gas  
 176 [31, 32]. The observed fluctuations in required voltage can be explained as bubbles are  
 177 formed on the electrode surface, especially at Cu<sub>2</sub>O-based GDEs, where higher  
 178 potentials are required ( $E= -1.25$  to  $-1.50$  V vs. Ag/AgCl), in comparison to the  
 179 application of Cu<sub>2</sub>O/ZnO mixtures airbrushed onto the carbon papers ( $E= -1.16$  V vs.  
 180 Ag/AgCl). The lower potentials needed for Cu<sub>2</sub>O-ZnO mixtures are in agreement with  
 181 the higher cyclic voltammetry responses reported for Cu<sub>2</sub>O/ZnO-based electrodes in  
 182 comparison to those electrodes with deposited Cu<sub>2</sub>O particles, denoting the synergic  
 183 effect of Cu<sub>2</sub>O and ZnO in the current-potential reduction response [11].

184 Moreover, the rate of CH<sub>3</sub>OH formation,  $r$ , decreased for both electrodes as time went  
 185 on, and then stabilize uniquely for Cu<sub>2</sub>O/ZnO layers after 30 minutes of reaction at  $r=$   
 186  $\sim 4 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  until the end of the experiment. Probably, at the first experimental  
 187 minutes, the electrolyte penetrated into the internal structure of the GDE, enlarging the  
 188 contact area. This may explain the enhanced reaction rate at 15 min of operation,

189 indicating that the structure is sufficiently soaked and the three-phase liquid films had  
 190 totally formed thoroughly the whole GDEs [33]. After this point, the GDE probably was  
 191 to wet, limiting mass transfer to some extent and accumulating liquid-phase reaction  
 192 products, which can partially block the electrode and reduce its electrochemically-active  
 193 surface area [34-36]. Therefore, a gradual infiltration of electrolyte may be preferred for  
 194 an enhanced CO<sub>2</sub> conversion at GDEs.

195 Table 1 shows the catalyst weight of the Cu-based samples after 30, 90 and 120 min of  
 196 CO<sub>2</sub> electroreduction time. The total weight of catalyst placed in the carbon paper was  
 197 10 mg and 20 mg for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, respectively.

198 **Table 1.** Particle loss for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO GDEs before and after a CO<sub>2</sub> electroreduction period  
 199 of 30, 90 and 120 min.

200

| Electrode             | Time (min) | Catalyst weight (mg) |       | Weight loss (%) |
|-----------------------|------------|----------------------|-------|-----------------|
|                       |            | Initial              | Final |                 |
| Cu <sub>2</sub> O     | 30         |                      | 9.04  | 9.56            |
|                       | 60         | 10                   | 8.55  | 14.54           |
|                       | 90         |                      | 7.97  | 20.35           |
| Cu <sub>2</sub> O/ZnO | 30         |                      | 19.04 | 4.82            |
|                       | 60         | 20                   | 18.72 | 6.41            |
|                       | 90         |                      | 18.61 | 6.97            |

201

202 The results confirmed the more stable properties of Cu<sub>2</sub>O/ZnO surfaces in comparison  
 203 to the Cu<sub>2</sub>O-based electrode, where the catalysts may be gradually peeled off from the  
 204 carbon paper. Besides, defects in the catalytic layer would likely assist tunnelling and an  
 205 increase the unwanted hydrogen formation due to easy access of water to catalytic sites.  
 206 Therefore, a uniform and defect free catalytic layer is desired [16, 21]. According to the  
 207 results, it is expected that Cu<sub>2</sub>O/ZnO layer could remain and catalyse the CO<sub>2</sub>  
 208 electroreduction for over 20 h (if we consider the same particle detachment rate), since  
 209 the total particle loss at 90 min was 1.39 mg of a total of 20 mg sprayed in the electrode.  
 210 Overall, even if the Cu<sub>2</sub>O-based GDEs present an initial better performance for CH<sub>3</sub>OH  
 211 formation, the utilization of Cu<sub>2</sub>O-ZnO mixtures is recommended for a continuous CO<sub>2</sub>  
 212 electrochemical conversion due to its stable properties with time.

213 The averaged formation rate for Cu<sub>2</sub>O/ZnO surfaces at 90 min of operation takes the  
214 value of  $r = 4.74 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ , which is higher than that value reported in our  
215 previous work at Cu<sub>2</sub>O/ZnO particles deposited onto carbon papers (without the supply  
216 of CO<sub>2</sub> gas),  $r = 3.17 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  [11]. Besides, the stable formation rate obtained  
217 at Cu<sub>2</sub>O/ZnO-based electrode is in the range of those values previously reported for air-  
218 furnace oxidized Cu foils ( $r = 2.36 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) and electrochemical oxidized Cu  
219 foils ( $r = 2.78 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) at potentials ranging from -1.2 to -1.5 V vs. Ag/AgCl  
220 [21] or the CH<sub>3</sub>OH formation rates reached at electrodes based on Cu<sub>2</sub>O  
221 electrodeposited on stainless steel,  $r = 11.9 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  at -1.05 V vs. Ag/AgCl  
222 [25].

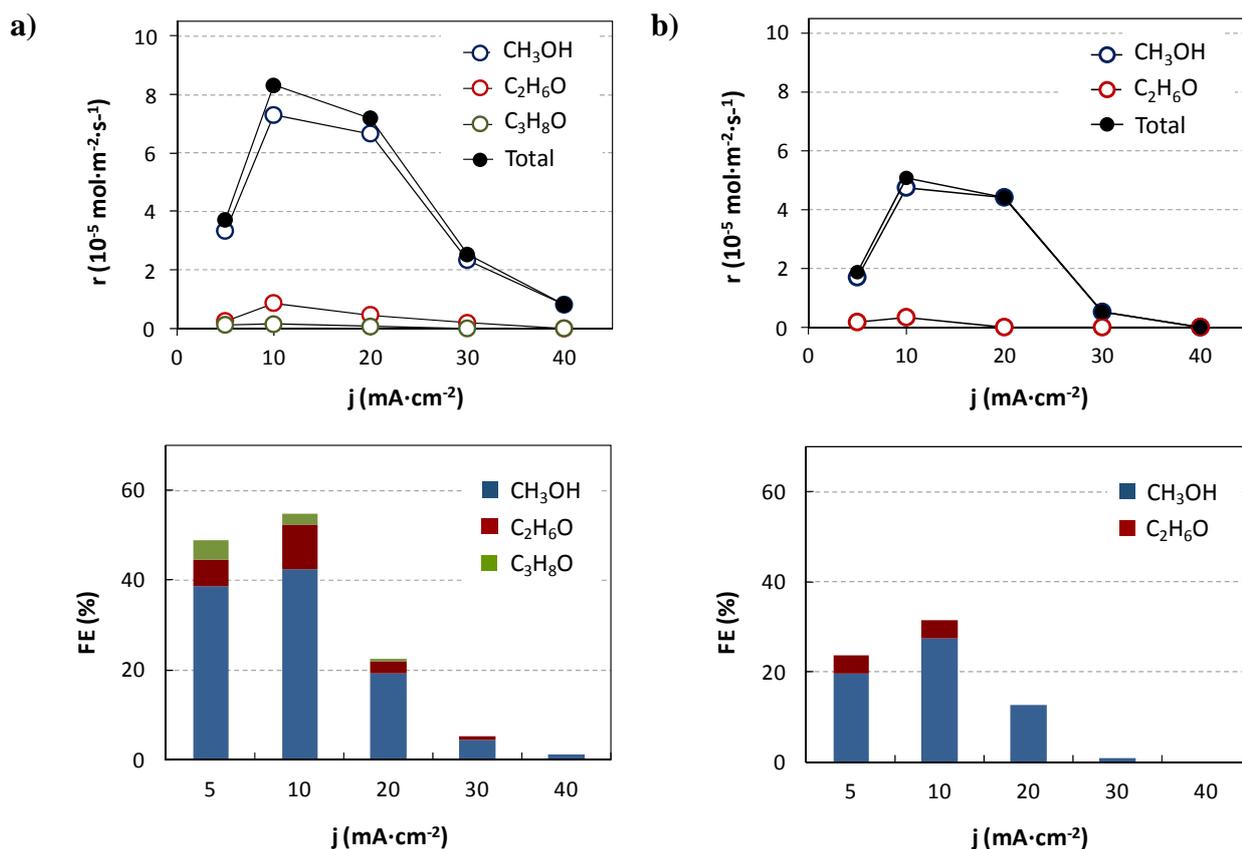
### 223 3.2. Key variables on the CO<sub>2</sub> electroreduction process

224 This section analyzes the influence of current density,  $j$ ; electrolyte flow/area ratio  
225 ( $Q_e/A$ ) and gas flow/area ratio ( $Q_g/A$ ) in the liquid-phase product distribution and the  
226 CO<sub>2</sub> conversion efficiency for the filter-press electrochemical system in continuous  
227 operation.

#### 228 3.2.1. Influence of current density

229 Figure 3 shows the quantitative information ( $r$  and  $FE$ ) regarding the liquid-phase  
230 product distribution at different current densities ( $j = 5$  to  $40 \text{ mA} \cdot \text{cm}^{-2}$ ).  $FE$  was  
231 calculated considering 6 electrons step pathways of CO<sub>2</sub> reduction to CH<sub>3</sub>OH, 12  
232 electrons required per molecule of ethanol (C<sub>2</sub>H<sub>6</sub>O) and 18 to produce n-propanol  
233 (C<sub>3</sub>H<sub>8</sub>O). A constant electrolyte flow/area ratio ( $Q_e/A$ ) and gas flow/area ratio ( $Q_g/A$ ) of  
234 2 and  $20 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$ , respectively, were applied in the tests. It may be noted that the  
235 carbon paper without metallic particles supported did not produce any measurable liquid  
236 product.

237



**Fig. 3.** Rates of product formation,  $r$ , and Faraday efficiencies,  $FE$ , for the major products obtained from  $\text{CO}_2$  electroreduction at (a)  $\text{Cu}_2\text{O}$  and; (b)  $\text{Cu}_2\text{O}/\text{ZnO}$ -GDEs as a function of current density applied.

238

239 The figures show that the product distribution and process efficiency is on dependence  
 240 of the current density applied. The system predominantly produces  $\text{CH}_3\text{OH}$ , with  
 241  $\text{C}_2\text{H}_6\text{O}$  as the second main product (which is a difficult reaction with 12 electrons  
 242 transfer required). The literature shows that the formation of  $\text{C}_2\text{H}_6\text{O}$  at Cu-based  
 243 electrodes is not unexpected [9, 37-42]. For example, Chi et al. [38] reported a good  
 244 selectivity for the formation of  $\text{C}_2\text{H}_6\text{O}$  ( $FE=15.5\%$ ) for CuO nanoparticles deposited on  
 245 carbon papers when using a 0.2 M  $\text{KHCO}_3$  solution. Trace amounts of  $\text{CH}_3\text{OH}$  and  
 246  $\text{C}_3\text{H}_8\text{O}$  were also detected. Ren et al. [40] recently reported the formation of C  
 247 compounds ( $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_2\text{H}_4$ ) on  $\text{Cu}_2\text{O}$  films at various electrochemical potentials. The  
 248  $FE$  was in the range of 9-16% for  $\text{C}_2\text{H}_6\text{O}$  formation in a 0.1 M  $\text{KHCO}_3$  electrolyte.  
 249 They hypothesized that  $\text{CO}_2$  is reduced through proton-electron transfer to give  $\text{HCOO}^-$   
 250 surface moiety, which can then hydrogenate to give  $\text{H}_2\text{O}$  and  $\text{CO}$  (adsorbed) at the  
 251 copper surface. These species can further hydrogenate to form  $\text{CH}_4$  or undergo  
 252 intermolecular C-C bond formation ( $\text{C}_1$  dimerization/hydrogenation) to yield  $\text{C}_2\text{H}_n\text{O}_2$   
 253 ( $n=0-4$ ), which is further reduce to  $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_2\text{H}_4$ . The  $\text{Cu}^+$  ions were postulated to

254 be the catalytic active for reducing CO<sub>2</sub> to C<sub>2</sub> compounds. Besides, Li and co-workers  
255 demonstrated that Cu<sub>2</sub>O films could reduce CO to C<sub>2</sub>H<sub>6</sub>O with a *FE* of 43% [41]. The  
256 metal particles boundaries on the surface (with undercoordinated Cu atoms) of the films  
257 were suggested to be the driving forces for C<sub>1</sub> dimerization to form C<sub>2</sub> products.  
258 Moreover, Kuhl et al. [9] evaluated the electrochemical reduction of CO<sub>2</sub> on a Cu  
259 surface across a range of potentials and observed a total of 16 different CO<sub>2</sub> reduction  
260 products (including CH<sub>3</sub>OH, C<sub>2</sub>H<sub>6</sub>O and C<sub>3</sub>H<sub>8</sub>O). They discuss a scheme for the  
261 formation of multicarbon products and recognized that all the C<sub>2</sub> and C<sub>3</sub> products  
262 detected may have been produced via the dehydroxylation of an earlier, less reduced  
263 product in its enol or diol form. Therefore, they hypothesized that the chemistry to  
264 generate the wide range of multicarbon products may occur through an enol-like surface  
265 intermediate, that desorb to convert to its diol and/or keton form. The presence of  
266 hydroxyl and/or carbonyl moieties in many of the C<sub>2</sub> and C<sub>3</sub> products suggest that the  
267 C-C coupling step occurs before at least one of the two carbon-oxygen bonds in CO<sub>2</sub> is  
268 broken. In any case, the mechanisms involved in C-C coupling reactions to form C<sub>2</sub> and  
269 C<sub>3</sub> products are still unclear. Certainly, further experimental work is needed to fully  
270 elucidate CO<sub>2</sub> reduction steps on Cu surfaces.

271 The results also suggest that the reaction conditions created in the GDEs may be able to  
272 vary product selectivity if we compare the results with those obtained at identical  
273 catalytic materials but without CO<sub>2</sub> supplied as gas, where CH<sub>3</sub>OH was the main  
274 product, and only trace amounts of C<sub>2</sub>H<sub>6</sub>O were detected [11]. This is not exceptional if  
275 we consider those results obtained by Kas et al. for electrodes prepared with Cu  
276 nanoparticles for CO<sub>2</sub> electroreduction to hydrocarbons [39, 42]. They proved that  
277 identical electrodes could yield predominately CH<sub>4</sub> and C<sub>2</sub>H<sub>4</sub> depending on process  
278 conditions, such as the applied CO<sub>2</sub> pressure, that can modify the conditions in the  
279 vicinity of the catalytic material. In theory, the GDE configuration changes CO<sub>2</sub> transfer  
280 radically. Owing to the abundant pores in the GDEs, CO<sub>2</sub> can diffuse to the electrode  
281 surface more conveniently than that from the bulk. Moreover, CO<sub>2</sub> in the reaction can  
282 be obtained from CO<sub>2</sub> (gas), rather than CO<sub>2</sub> (aqueous) by use of GDEs, so that the  
283 concentration of CO<sub>2</sub> (adsorbate) on the electrode surface can be increased [34] which  
284 probably may lead to the formation of more reduced species, altering the distribution of  
285 products from the reaction. It is also interesting to note the positive effects of supplying  
286 a CO<sub>2</sub> gas flow through the electrode structure, which may provoke that the liquid

287 products diffuse more easily to the solution, avoiding the entrapment of liquid products  
 288 into the carbon paper porous structure. Further research is required to fully understand  
 289 this phenomenon.

290 Figure 3a and b reveal that the total rate of CO<sub>2</sub> reduction to liquid-phase products,  $r_T$ ,  
 291 did not improve at current densities higher than  $j = 10 \text{ mA}\cdot\text{cm}^{-2}$ , where a maximum  
 292 value of  $r_T = 8.32 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  and  $r_T = 5.08 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  can be obtained at  
 293 Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, respectively. In addition, the overall  $FE_T$  (the  
 294 results of cumulative efficiencies for the formation of the different products) fell  
 295 drastically as the current was increased from  $j = 10$  to  $40 \text{ mA}\cdot\text{cm}^{-2}$ . This may be  
 296 explained as the additional current density applied is consumed by side reactions, such  
 297 as the production of hydrogen (which competes with the electroreduction of CO<sub>2</sub> to  
 298 useful products) and may indicate an optimal electrocatalytic current density of  $j = 10$   
 299  $\text{mA}\cdot\text{cm}^{-2}$ , where the overall efficiency values can be as high as  $FE_T = 54.8\%$  and  $31.4\%$   
 300 for the Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based surfaces, respectively.

301 Moreover, Table 2 compares the product distribution and  $FE$  for CO<sub>2</sub> conversion  
 302 obtained in the present work with those previously obtained for the same materials in a  
 303 CO<sub>2</sub>-saturated 0.5 M KHCO<sub>3</sub> solution (without CO<sub>2</sub> supplied as gas) [11]. The  
 304 performance is, at the same time, compared with the values obtained in a CO<sub>2</sub>-saturated  
 305 0.5 M KHCO<sub>3</sub> solution when N<sub>2</sub> gas is supplied through the GDE structure (instead of  
 306 CO<sub>2</sub>).

307 **Table 2.** Electrochemical reduction of CO<sub>2</sub> at Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO electrodes when CO<sub>2</sub> and N<sub>2</sub> gas flow  
 308 through the GDE, and when no gas is supplied. Electrolyte flow/area ratio ( $Q_e/A$ ) =  $2 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ . Gas  
 309 flow ratio ( $Q_g/A$ ) =  $20 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ .

| Electrode             | Flowing gas     | $j \text{ (mA}\cdot\text{cm}^{-2})$ | $E \text{ vs. Ag/AgCl}$ | FE (%)             |                                 |                                 |       |
|-----------------------|-----------------|-------------------------------------|-------------------------|--------------------|---------------------------------|---------------------------------|-------|
|                       |                 |                                     |                         | CH <sub>3</sub> OH | C <sub>2</sub> H <sub>6</sub> O | C <sub>3</sub> H <sub>8</sub> O | Total |
| Cu <sub>2</sub> O     | CO <sub>2</sub> | 10                                  | 1.39                    | 42.3               | 10.1                            | 2.4                             | 54.8  |
|                       | N <sub>2</sub>  | 10                                  | 1.52                    | 40.2               | 2.3                             | -                               | 42.5  |
|                       | -               | 6.93 <sup>a</sup>                   | 1.30                    | 45.7               | Trace                           | -                               | 45.7  |
| Cu <sub>2</sub> O/ZnO | CO <sub>2</sub> | 10                                  | 1.16                    | 27.5               | 3.9                             | -                               | 31.4  |
|                       | N <sub>2</sub>  | 10                                  | 1.69                    | 18                 | 1.5                             | -                               | 19.5  |
|                       | -               | 10.64 <sup>a</sup>                  | 1.30                    | 17.7               | Trace                           | -                               | 17.7  |

310 <sup>a</sup> Data from ref. [11]

311 The overall  $FE$  achieved for the conversion of  $CO_2$  demonstrated that the GDE with  
312  $CO_2$  gas feeding to the electrocatalysts contributed to the high electrolysis efficiency, as  
313 compared to those results obtained at the identical electrodes when no  $CO_2$  as gas is  
314 supplied [11]. Besides, as observed from the results, the  $Cu_2O$ -GDE maintained a higher  
315 efficiency for  $CO_2$  reduction ( $FE_T= 54.8\%$ ) at higher current density ( $j=10 \text{ mA}\cdot\text{cm}^{-2}$ )  
316 than at  $Cu_2O$ -surfaces ( $FE_T= 45.7\%$ ) at lower current applied ( $j= 6.93 \text{ mA}\cdot\text{cm}^{-2}$ ). This  
317 may indicate that the application of GDEs (with  $CO_2$  supplied as gas) is advantageous,  
318 since the process can be operated at higher current densities, while yielding higher  $CO_2$   
319 reduction efficiencies.

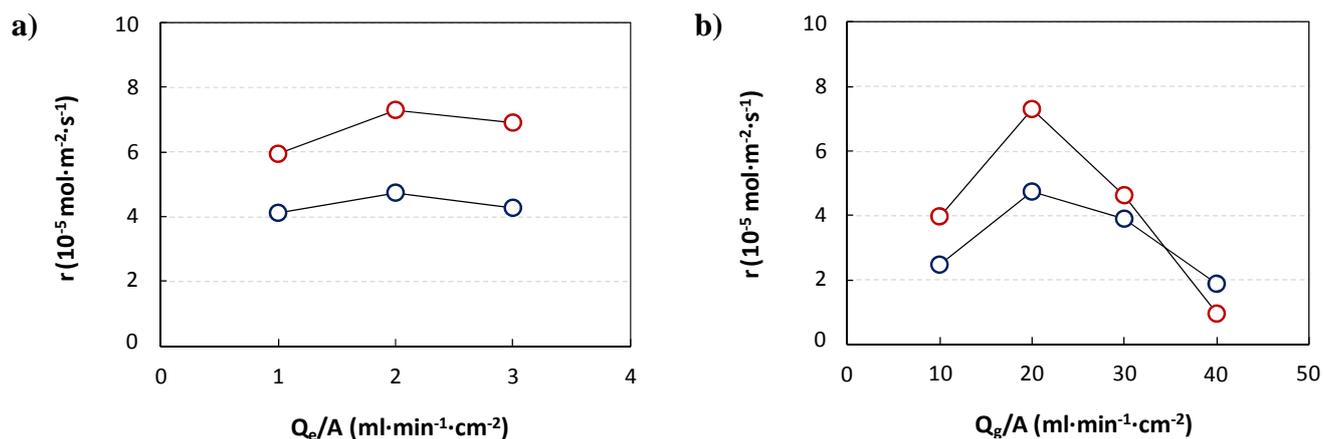
320 Moreover, the efficiency values for the conversion of  $CO_2$  at GDEs are remarkably  
321 higher than those values obtained at a  $CO_2$ -saturated solution when  $N_2$  gas is supplied  
322 through the GDE structure, which suggest that the conversion of  $CO_2$  molecule can be  
323 not uniquely attributed to an enhanced agitation and diffusion of reactants in the  
324 electrochemical cell, but also to an increase of  $CO_2$  (adsorbate) available on the catalytic  
325 surface, leading to more reduced species.

### 326 *3.2.2. Influence of electrolyte flow rate ( $Q_e/A$ ) and gas flow rate ( $Q_g/A$ )*

327 In our previous study, external mass transfer limitations were detected in the filter-press  
328 electrochemical cell system [11], which might be overcome with the application of  
329 GDEs [13-16]. In order to improve the  $CO_2$  electroreduction performance, additional  
330 experiments were carried out at different electrolyte flow/area ratio ( $Q_e/A$ ) and  $CO_2$  gas  
331 flow/area ratio ( $Q_g/A$ ) and the results for the formation of the major product,  $CH_3OH$ ,  
332 are presented in Figure 4a and b, respectively.

333

334



**Fig. 4.** Rate for CO<sub>2</sub> reduction to CH<sub>3</sub>OH,  $r$ , at (a) different electrolyte flow rate ( $Q_e/A$ ) and; (b) CO<sub>2</sub> gas flow rate ( $Q_g/A$ ) at the Cu<sub>2</sub>O (in red) and Cu<sub>2</sub>O/ZnO (in blue) GDEs. Current density:  $j= 10 \text{ mA}\cdot\text{cm}^{-2}$

335

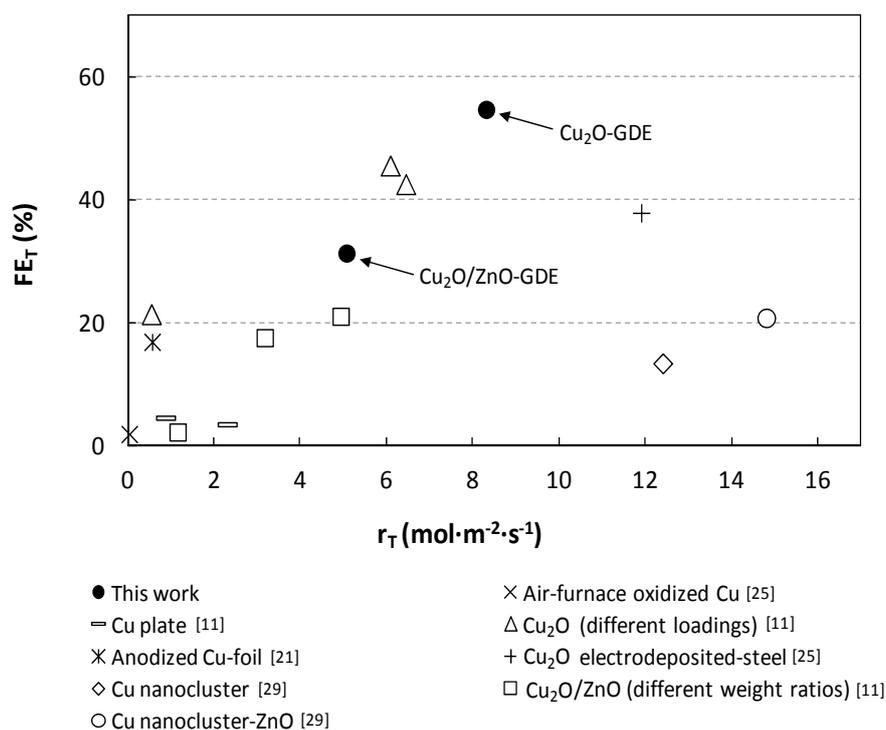
336 Firstly, Figure 4a shows that increases in  $Q_e/A$  from 1 to 3 ml·min<sup>-1</sup> did not produce a  
 337 significant alteration in the rate of CO<sub>2</sub> electrochemical conversion to CH<sub>3</sub>OH, which  
 338 indicated that using low  $Q_e/A$  ratios is preferred in the GDE system since a more  
 339 concentrated product can be obtained without sacrificing the rate of CH<sub>3</sub>OH formation  
 340 (i.e. from 4.56 to 2.74 mg·l<sup>-1</sup> at  $Q_e/A= 2$  and 3 ml·min<sup>-1</sup>, respectively, at Cu<sub>2</sub>O/ZnO  
 341 GDE). Besides, lower electrolyte flows may allow a gradual infiltration of catholyte in  
 342 the GDE structure, which is preferred for an enhanced CO<sub>2</sub> electroreduction, as  
 343 discussed in section 3.1. Therefore, since process performance was only slightly  
 344 affected by the electrolyte flow, it can be concluded that the process may be primarily  
 345 limited by the internal diffusion of reactants through the porous structure of the GDE,  
 346 where the metal particles are deposited [13].

347 Additionally, Figure 4b demonstrated the importance of adjusts the optimal CO<sub>2</sub> gas  
 348 flow process. The lower formation rate ( $r= 2.48 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ ) for Cu<sub>2</sub>O/ZnO-based  
 349 electrode at  $Q_g/A= 10 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$  in comparison to that value at  $Q_g/A= 20 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$   
 350 ( $r= 4.74 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ ) indicated that the process is clearly limited by the  
 351 CO<sub>2</sub> gas supplied to the system. On the other hand, the application of a high CO<sub>2</sub> gas  
 352 flow of  $Q_g/A= 40 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$  produced a severe decrease in the formation rate for  
 353 both electrodes, which can be partially attributed to the rapid detachment of metal  
 354 particles at these relatively high gas flows applied, in accordance with the main stability  
 355 limitations observed in GDE systems [15, 31, 43].

356 Therefore, the optimal point should provide enough CO<sub>2</sub> gas supply for the reaction,  
357 well before a massive detachment of metal particles occurs. This seems to happen at a  
358 flow range between  $Q_g/A= 20$  to  $30 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ . These results are interesting and  
359 should be taken into account in order to design efficient processes for CO<sub>2</sub>  
360 eletroreduction to CH<sub>3</sub>OH at GDE-based systems.

### 361 3.3. Comparison with other electrocatalytic materials

362 Finally, the results obtained in the present work for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-GDEs are  
363 compared with previous results for CO<sub>2</sub> electroreduction to liquid products at different  
364 Cu-based materials (when boht,  $r$  and  $FE$ , values available) at an applied potential range  
365 of  $E= -1$  to  $-1.5$  vs. V Ag/AgCl [11, 21, 25, 29]. Figure 5 represents the total rate of CO<sub>2</sub>  
366 conversion,  $r_T$ , vs. cumulative Faradaic efficiency,  $FE_T$ , reported in the literature for the  
367 formation of different liquid-phase products, including CH<sub>3</sub>OH. The figure uniquely  
368 provide a picture for comparison of CO<sub>2</sub> electroreduction performance, although other  
369 variables such as reaction medium, operating conditions and/or cell/electrode structure  
370 were applied, which may affect the results. The extraordinary high FE (i.e. >100%),  
371 where obviously both chemical and electrochemical steps involved in the CO<sub>2</sub> reduction  
372 process, obtained at anodized Cu foils and pre-oxidized Cu-TiO<sub>x</sub> electrodes [21] have  
373 been not included in order to clarify the analysis.



**Fig. 5.** Total rate of CO<sub>2</sub> conversion to liquid-phase products,  $r_T$ , vs. Faradaic efficiency,  $FE_T$ , for different Cu-based materials at E= -1 to -1.5 V vs. Ag/AgCl

374

375 As can be seen from the figure, the total CO<sub>2</sub> conversion efficiency obtained for GDEs  
 376 in the present work outperformed those values observed at Cu, oxidized Cu and Cu-Zn  
 377 surfaces, which may denote the positive effect of using GDEs. Nevertheless, the rate of  
 378 CO<sub>2</sub> reduction to useful products is still below those values reported for Cu<sub>2</sub>O  
 379 electrodeposited-steel electrode,  $r_T = 11.9 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  at -1.05 V vs. Ag/AgCl [25]  
 380 or those values for Cu nanoclusters-ZnO mixtures at -1.4 V, where high total formation  
 381 rates,  $r_T = 12.4 - 14.8 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ , were reached. In any case, the relatively high  
 382 CO<sub>2</sub> conversion rate to liquid products,  $r_T = 5.08 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  and total Faradaic  
 383 efficiency,  $FE_T = 31.4\%$ , as well as the stable behavior, suggest the use of Cu<sub>2</sub>O/ZnO-  
 384 based GDEs for the continuous electrochemical reduction of CO<sub>2</sub> to useful products,  
 385 where CH<sub>3</sub>OH is the predominant product.

386 Future research should probably include the development of new highly active catalysts,  
 387 as well as a deeper study to understand the relationship between GDE morphology and  
 388 effective gas-liquid separation, while facilitating transport of reactants and products.  
 389 These progresses may lead in the near future to an economically-viable CO<sub>2</sub>  
 390 electrochemical process in continuous operation.

#### 391 4. Conclusions

392 This work demonstrated that the electroreduction of CO<sub>2</sub> to liquid products can be  
393 effectively carried out in continuous in a filter-press electrochemical cell equipped with  
394 Cu<sub>2</sub>O-based gas-diffusion electrodes (GDEs). The GDE configuration allows breaking  
395 through the mass transfer limitations usually found in electroreduction systems,  
396 producing an enhanced CO<sub>2</sub> reduction performance. The study included the  
397 experimental evaluation of key variables (i.e. current density,  $j$ ; electrolyte flow/area  
398 ratio,  $Q_e/A$ ; and CO<sub>2</sub> gas flow rate/area ratio,  $Q_g/A$ ) for the electrochemical conversion  
399 of CO<sub>2</sub> at Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO commercial particles deposited onto carbon papers in a  
400 0.5 M KHCO<sub>3</sub> catholyte under ambient conditions.

401 The experimental results in the filter-press electrochemical cell revealed that  
402 Cu<sub>2</sub>O/ZnO-GDEs are expected to remain stable over 20 h, in contrast to Cu<sub>2</sub>O surfaces  
403 that suffered a strong deactivation with time. The analysis of the liquid catholyte  
404 demonstrated that methanol was formed predominantly, with small amounts of ethanol  
405 and n-propanol.

406 The overall formation rate for the formation of liquid-phase products did not improve at  
407 current densities higher than  $j= 10 \text{ mA}\cdot\text{cm}^{-2}$ , where a maximum value of  $r_T= 5.08 \times 10^{-5}$   
408  $\text{mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  was obtained at Cu<sub>2</sub>O/ZnO-GDEs. In addition, the overall *FE* (the results of  
409 cumulative efficiencies for the formation of the different products) fell drastically as the  
410 current was increased from  $j= 10$  to  $40 \text{ mA}\cdot\text{cm}^{-2}$ . The process performance was not  
411 affected by electrolyte flow, suggesting that the process may be primarily limited by the  
412 internal diffusion of reactants through the porous structure of the GDE, where the metal  
413 particles are deposited. In addition, the results demonstrated the importance of adjusting  
414 the optimal CO<sub>2</sub> gas flow in the electrochemical cell in order to supply enough CO<sub>2</sub> to  
415 react before a rapid detachment of metal particles from the catalytic surface occurred.  
416 Thus, the maximum efficiency detected at Cu<sub>2</sub>O/ZnO surfaces was  $FE_T= 31.4\%$  (at  $j=$   
417  $10 \text{ mA}\cdot\text{cm}^{-2}$ ,  $Q_e/A= 2 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$  and  $Q_g/A= 20 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ ), which is a  
418 significantly higher value than those results previously reported in literature for Cu-  
419 based electrodes and show the potential of Cu<sub>2</sub>O/ZnO-GDEs for the effective  
420 electrochemical valorization of CO<sub>2</sub>.

421 Overall, the results presented in this work are promising, but research efforts must be  
422 continued in order to develop new electroreduction systems based on highly active,

423 selective and stable materials to overcome the current limitations of the process before  
424 practical applications.

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