



Published in final edited form as:

Chem Eng J. 2018 December 1; 353: 657–665. doi:10.1016/j.cej.2018.07.124.

## Insight on the generation of reactive oxygen species in the $\text{CaO}_2/\text{Fe(II)}$ Fenton system and the hydroxyl radical advancing strategy

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### Abstract

Calcium peroxide ( $\text{CaO}_2$ ) is a stable hydrogen peroxide ( $\text{H}_2\text{O}_2$ ) carrier, and the  $\text{CaO}_2/\text{Fe(II)}$  system has been applied for treatment of various pollutants. It is commonly reported in the literature that hydroxyl radical ( $\text{HO}^\bullet$ ) and superoxide radical anions ( $\text{O}_2^{\bullet-}$ ) are the two main reactive oxygen species (ROSs) generated in the  $\text{CaO}_2/\text{Fe(II)}$  system. However, many of the reported results were deduced from degradation performance rather than specific testing of radical generation. Thus, the specific generation of ROSs and the influence of system conditions on ROSs yield is still unclear. To our knowledge, this is the first study specifically focusing on the generation of  $\text{HO}^\bullet$  and  $\text{O}_2^{\bullet-}$  in the  $\text{CaO}_2/\text{Fe(II)}$  system. Experimental conditions were optimized to investigate the production of  $\text{HO}^\bullet$  and  $\text{O}_2^{\bullet-}$ . The results showed the influences of  $\text{CaO}_2$ ,  $\text{Fe(II)}$ , and solution pH on  $\text{HO}^\bullet$  and  $\text{O}_2^{\bullet-}$  generation, and the  $\text{HO}^\bullet$  generation efficiency was reported for the first time. In addition, the ROSs generation pathways in the  $\text{CaO}_2/\text{Fe(II)}$  system were elucidated. A strategy for enhancing  $\text{HO}^\bullet$  yield is developed, based on the continuously dosing  $\text{Fe(II)}$ . This proposed strategy has implications for the effective application of *in situ* chemical oxidation employing  $\text{CaO}_2/\text{Fe(II)}$  for groundwater remediation.

### Keywords

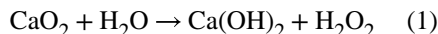
Hydroxyl radical; Superoxide radical anion;  $\text{CaO}_2/\text{Fe(II)}$  oxidation; ROSs yield; *In situ* chemical oxidation

## 1. Introduction

Due to the instability of liquid  $\text{H}_2\text{O}_2$  in the subsurface, the use of the conventional Fenton reaction for *in situ* remediation applications is limited. This has led to the development of

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stable H<sub>2</sub>O<sub>2</sub> sources for subsurface applications. It has been reported that calcium peroxide (CaO<sub>2</sub>) can produce H<sub>2</sub>O<sub>2</sub> over a wide pH range (Eq. 1).

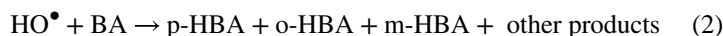


As a solid, not all of the contained H<sub>2</sub>O<sub>2</sub> is available at once. Hence, the slow release of H<sub>2</sub>O<sub>2</sub> from CaO<sub>2</sub> can reduce unexpected H<sub>2</sub>O<sub>2</sub> loss, making CaO<sub>2</sub> a more effective source of H<sub>2</sub>O<sub>2</sub> than liquid H<sub>2</sub>O<sub>2</sub>. For example, Northup and Cassidy [1] reported that CaO<sub>2</sub> was a more efficient oxidant than liquid H<sub>2</sub>O<sub>2</sub> at pHs greater than 6 for the treatment of tetrachloroethene. Similarly, Bogan et al. [2] found that the removal efficiency was enhanced from 5% to 44% after the substitution of H<sub>2</sub>O<sub>2</sub> with CaO<sub>2</sub> in the treatment of polycyclic aromatic hydrocarbons (PAHs). Moreover, CaO<sub>2</sub> has been used in removing endocrine disrupting compounds, cable insulating oil, toluene, trichloroethylene, benzene, and other organics [3–7]. The treatment process using CaO<sub>2</sub> alone is relatively inefficient, and the introduction of Fe(II) can greatly accelerate the process [6,7].

Prior research has reported that hydroxyl radical (HO<sup>•</sup>) and superoxide radical anions (O<sub>2</sub><sup>•-</sup>) as the probable reactive oxygen species (ROSs) produced in CaO<sub>2</sub> based oxidation systems [5–9]. However, many of the reported results were deduced from degradation performance rather than specific testing of radical generation. Thus, the specific generation of ROSs and the influence of system conditions on ROSs yield is still unclear. In addition, several factors common to oxidation experiments can obscure the identification and quantification of ROSs. First, it is possible that intermediate radicals may also contribute to contaminant degradation [10]. Second, the presence of other constituents, such as catalysts, salts, co-contaminants, degradation intermediaries, and dissolved organic carbon, can compete with the target compound for the ROSs [6,7,9–12]. Although the degradation performance can provide information about the primary ROS involved, the results are uncertain. So far, there are few studies focusing on the generations of these ROSs in the CaO<sub>2</sub> based Fenton system, particularly regarding generation efficiency of HO<sup>•</sup>. Such information is required to support the efficient use of ROSs in the CaO<sub>2</sub>/Fe(II) Fenton system. Thus it is critical to design experiments specifically for evaluating the generation of HO<sup>•</sup> and O<sub>2</sub><sup>•-</sup> and investigating the influence of solution chemistry to improve our understanding of the CaO<sub>2</sub>/Fe(II) Fenton system for application to contamination remediation.

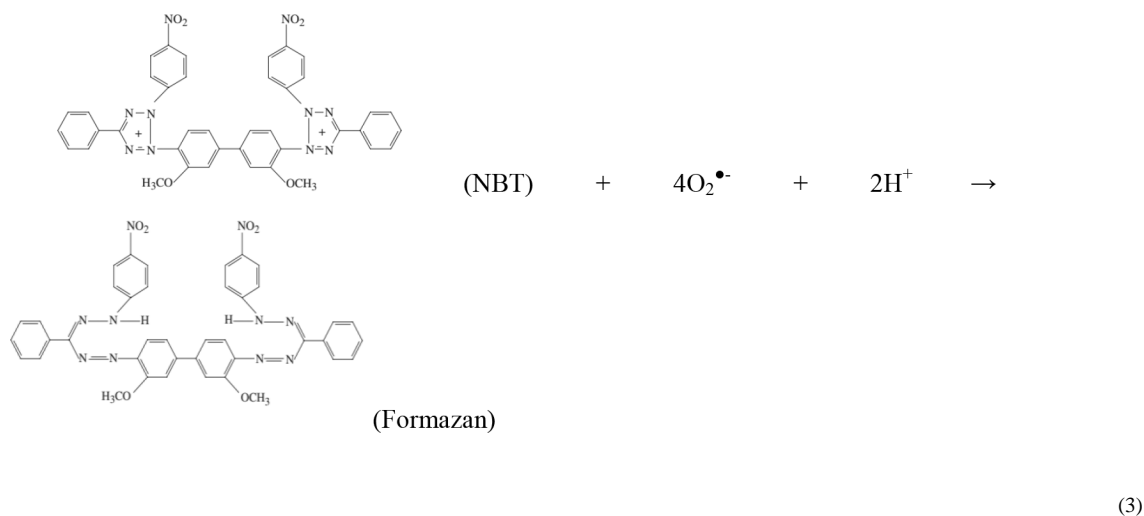
The radical-specific probe analysis approach can be used to characterize radical generation [13–15]. For HO<sup>•</sup>, the frequently used probe compounds include coumarin [16–18], salicylic acid [19–21], benzoic acid (BA) [14,22], 1-propanol [22], and their reaction rate constants with HO<sup>•</sup> are listed in Table 1 [22]. Conversely, luminol [24,25], methoxy cypiridina luciferin analog (MCLA) [26], and various tetrazolium salts including nitroblue tetrazolium (NBT) [27–29] and 2,3-bis (2-methoxy-4-nitro-5-sulfophenyl)-2H-tetrazolium-5-carboxanilide (XTT) [30] have been used in determining O<sub>2</sub><sup>•-</sup> generation in various systems. The advantages and disadvantages of the probes in O<sub>2</sub><sup>•-</sup> determination are also listed in Table 1.

In this study, BA is used as a probe to study the generation of  $\text{HO}^\bullet$  in the  $\text{CaO}_2/\text{Fe(II)}$  Fenton system. It is reported that the reaction between BA and  $\text{HO}^\bullet$  produces p-hydroxybenzoic acid (p-HBA), o-HBA, m-HBA, and other products (Eq. 2).



Zhou and Mopper [14] reported that p-, o- and m-HBA accounted for  $90 \pm 5\%$  of the products from the reaction between  $\text{HO}^\bullet$  and BA. They also found that the detected sensitivity of p-HBA is higher than other isomers, and that it can be used for the calculation of  $\text{HO}^\bullet$  generation with the conversion factor of  $5.87 \pm 0.18$ . This method has been employed to quantify  $\text{HO}^\bullet$  generated in Fenton systems [22,31] and other advanced oxidation processes (AOPs) [16,32–35]. However, it should be noted that  $\text{HO}^\bullet$  radicals will react with not only BA, but also other substances such as iron ions, residual  $\text{H}_2\text{O}_2$ ,  $\text{HO}^\bullet$  radicals. In other words, the measured  $\text{HO}^\bullet$  is the cumulative capability for production and consumption of  $\text{HO}^\bullet$  in the  $\text{CaO}_2/\text{Fe(II)}$  Fenton system at the sampling point. Furthermore, the expected concentration of p-HBA can be too low to proceed for further oxidation with  $\text{HO}^\bullet$ , showing the advantage of this technique in  $\text{HO}^\bullet$  quantification. Therefore, p-HBA can be applicable as an indicator to represent  $\text{HO}^\bullet$  generation capability and be helpful to compare the degradation potentials of the  $\text{CaO}_2/\text{Fe(II)}$  Fenton process in different operating conditions.

NBT does not react with  $\text{H}_2\text{O}_2$  and  $\text{HO}^\bullet$ , and has good selectivity in  $\text{O}_2^{\bullet-}$  determination and can be used in evaluating  $\text{O}_2^{\bullet-}$  even at low concentration [27]. Thus, NBT is used to study  $\text{O}_2^{\bullet-}$  generation in the  $\text{CaO}_2/\text{Fe(II)}$  Fenton system (Eq. 3).



NBT can be reduced by  $\text{O}_2^{\bullet-}$  forming insoluble formazan in aqueous solution, and formazan can be soluble in some aprotic solvents forming a purple solution [5,8]. In addition, the determination of  $\text{O}_2^{\bullet-}$  can be confirmed by the absorbance of residual NBT solution or the formation of formazan, as shown in Table 1. Ma et al. used NBT to identify

the generation of  $\text{O}_2^{\bullet-}$  in the  $\text{CaO}_2$  system [8], and Qian et al. used NBT to determine  $\text{O}_2^{\bullet-}$  variation in a nano- $\text{CaO}_2$  system [5]. Although this method cannot quantify  $\text{O}_2^{\bullet-}$  yield, the results can provide comparable  $\text{O}_2^{\bullet-}$  concentration and characterize  $\text{O}_2^{\bullet-}$  variations as a function of experimental design.

Hence, in this study, we use the two above mentioned probes to study the ROSs produced in the  $\text{CaO}_2/\text{Fe(II)}$  system. This supports the deduction of the ROSs generation pathways. Based on the results, we propose an efficient strategy to enhance the  $\text{HO}^{\bullet}$  generation in the  $\text{CaO}_2$  based Fenton system.

## 2. Experiments

### 2.1 Experimental design

All experiments were performed in 250 mL glass vessels with a jacket for temperature control at  $20 \pm 2^\circ\text{C}$ . The materials used are listed in Supplementary Material (Text S1).

For  $\text{HO}^{\bullet}$  determination, a single dose of  $\text{CaO}_2$  and  $\text{Fe(II)}$  was added to BA solution with vigorous mixing. Control tests with the absence of  $\text{CaO}_2$  or  $\text{Fe(II)}$  were carried out in parallel. 2 mL samples were taken at the predetermined time and quenched by 0.1 mL 1-propanol, and followed by pH adjustment for reducing p-HBA loss in the filter. The treated samples were then acidized and analyzed by the high performance liquid chromatography (HPLC) to quantify  $\text{HO}^{\bullet}$  generation through p-HBA production between BA and  $\text{HO}^{\bullet}$  [18].

To evaluate  $\text{O}_2^{\bullet-}$ , a single dose of  $\text{CaO}_2$  and  $\text{Fe(II)}$  was added in ultrapure water with vigorous mixing. 5 mL samples were taken at the predetermined time and immediately mixed with 5 mL NBT solution [5]. The precipitant was dissolved in 5 mL ethanol, and then the organic phase was measured with DR-6000 spectrophotometer (HACH, USA).

BA and NBT solutions were equilibrated with ultrapure water. The fresh probe solutions were prepared daily. All the experiments were conducted twice and the mean values were presented.

### 2.2 Analytical methods

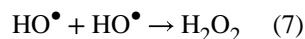
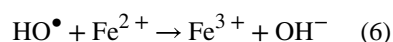
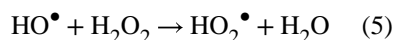
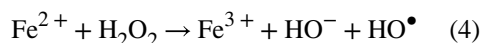
Analyses of BA and p-HBA were conducted by using an HPLC (Shimadzu LC-20AT, Japan) coupled with UV-vis detector (SPD-20A) and an auto-sampler (SIL-20A). A 10  $\mu\text{L}$  sample was injected into ODS-SP reversed-phase column (5  $\mu\text{m}$ , 4.6 mm  $\times$  250 mm). The isocratic eluent was a solvent mixture of 0.1% phosphoric acid (v/v) (A) and methanol (B), and the flow rate was 1.0 mL  $\text{min}^{-1}$ . p-HBA was quantified at 255 nm, and BA was quantified at 225 nm [18]. Both BA and p-HBA were stable during the whole analyses. In order to reduce the loss of BA and p-HBA, NaOH was used to raise the sample pH  $> 8$  before filtering a 0.22  $\mu\text{m}$  nylon filter (Aladdin, China), and the filtered solution was adjusted to pH 3 via  $\text{H}_2\text{SO}_4$  [20]. NBT-formazan was analyzed by spectrophotometer (DR-6000, HACH, USA) under the wavelength scanning mode. Ultrapure water was obtained from Class DI purification system (ELGA, 102 Marlow, UK).

H<sub>2</sub>O<sub>2</sub> was determined by spectrophotometric method [36], and the concentration of the available Fe(II) was determined according to the modified 1,10-phenanthroline method [37,38]. The solution pH was recorded by a pH meter equipped with a pH/ATC electrode (Sartorius, PB-10, Germany).

### 3. Results and Discussion

#### 3.1 HO<sup>•</sup> generation in the CaO<sub>2</sub>/Fe(II) Fenton system

The major HO<sup>•</sup> source in the CaO<sub>2</sub>/Fe(II) Fenton system is derived from the reactions as shown in Eqs. 1 and 4. There are also several reactions occurring simultaneously that act as HO<sup>•</sup> sinks (Eqs. 5–7). Fig. S1 shows the fate of HO<sup>•</sup> in the presence of BA in the CaO<sub>2</sub>/Fe(II) Fenton system. Due to the various sinks, a high concentration of probe is required in this study, and the reaction between HO<sup>•</sup> and the probe compound should be dominant, ensuring the reaction mirrors HO<sup>•</sup> generation [39].



The results of preliminary tests are shown in the Supplementary Material (Text S2, Fig. S2). Fig. S2a shows that HO<sup>•</sup> generation increased with increasing BA concentration, and Figs. S2b and 2c present the residual BA concentration. Fig. S3 displays the HPLC chromatograms of the p-HBA and BA when the molar ratio of CaO<sub>2</sub>/Fe(II)/BA was set at 1/1/10, which was selected as the control condition in the followed experiments. The results demonstrate that BA is a suitable probe compound for quantifying HO<sup>•</sup> in the CaO<sub>2</sub>/Fe(II) system, and the BA concentration is optimized and selected as 10 mM to trap HO<sup>•</sup> in the following experiments.

**3.1.1 The roles of CaO<sub>2</sub> and Fe(II) on HO<sup>•</sup> generation**—The control tests showed that CaO<sub>2</sub> or Fe(II) alone could not react with BA to generate p-HBA (Fig. 1), and that the reaction between CaO<sub>2</sub> and Fe(II) is the main source for HO<sup>•</sup> generation. Thus both CaO<sub>2</sub> and Fe(II) are the crucial factors affecting HO<sup>•</sup> yield.

Fig. 1 illustrates the effect of  $\text{CaO}_2$  dosage on  $\text{HO}^\bullet$  generation. The experiments were carried out with the varied  $\text{CaO}_2$  dosage from 0 to 4.0 mM, whilst fixing the initial  $\text{Fe(II)}$  concentration at 1.0 mM. Since  $\text{HO}^\bullet$  originated from the  $\text{CaO}_2/\text{Fe(II)}$  Fenton reaction, it was expected that the amount of  $\text{HO}^\bullet$  would proportionally increase with the increased dosage of  $\text{CaO}_2$ . As shown in Fig. 2, it is clear that the amount of  $\text{HO}^\bullet$  increased 2.9 fold when  $\text{CaO}_2$  concentration increased from 0.5 to 2.0 mM, and the depletion rate of  $\text{Fe(II)}$  was simultaneously increased from 0.069 to 0.085  $\text{mM min}^{-1}$  in the first 10 mins, and the production of  $\text{HO}^\bullet$  was accordingly enhanced. However, further increasing  $\text{CaO}_2$  concentration to 4.0 mM had less benefit to the generation of  $\text{HO}^\bullet$ . Though the depletion rate of  $\text{Fe(II)}$  was slightly increased from 0.085 to 0.087  $\text{mM min}^{-1}$  in the first 10 mins, the detected  $\text{H}_2\text{O}_2$  was doubled with a doubled  $\text{CaO}_2$  dosage of 4.0 mM (Fig. 2a). The excessive  $\text{H}_2\text{O}_2$  would also act as  $\text{HO}^\bullet$  sink which competed with BA for reaction with  $\text{HO}^\bullet$  (Eq. 5). Therefore, too much  $\text{CaO}_2$  could cause more useless  $\text{HO}^\bullet$  scavenging and less  $\text{HO}^\bullet$  production. Besides, the initially added  $\text{Fe(II)}$  will be oxidized to  $\text{Fe(III)}$  within minutes and thereafter the Fenton system will performance independent of the added  $\text{Fe(II)}$  presenting an initial burst of  $\text{HO}^\bullet$  [40–42].

Because  $\text{HO}^\bullet$  originated from  $\text{H}_2\text{O}_2$  decomposition catalyzed by  $\text{Fe(II)}$ ,  $\text{Fe(II)}$  dosage should have great influence on  $\text{HO}^\bullet$  generation. Fig. 1 shows the increase in  $\text{HO}^\bullet$  concentration from 0.29 to 0.32 mM after 60 min reaction when  $\text{Fe(II)}$  dosage increased from 0.5 to 1.0 mM. However, further increasing  $\text{Fe(II)}$  dosage to 4.0 mM reduced the generation of  $\text{HO}^\bullet$  to 0.24 mM. Figs. 2c and 2d show the changes of  $\text{H}_2\text{O}_2$  and  $\text{Fe(II)}$ . When  $\text{Fe(II)}$  dosage was 0.5 and 1.0 mM,  $\text{H}_2\text{O}_2$  increased in the initial 10 min and later declined significantly (Fig. 2c). It is noted that the variation of  $\text{Fe(II)}$  was quite different. With the increase of  $\text{Fe(II)}$  dosage, the consumption of  $\text{Fe(II)}$  rapidly rose in the initial 10 min and then exhibited a plateau (Fig. 2d). Further increasing  $\text{Fe(II)}$  dosage over 2.0 mM resulted in a different pattern. The consumption of  $\text{Fe(II)}$  was observed within the initial 5 min, while  $\text{H}_2\text{O}_2$  was not detected at the very beginning of the reaction (Fig. 2c). The rapid consumption of  $\text{Fe(II)}$  and  $\text{H}_2\text{O}_2$  indicates fast reactions, which could lead to a dramatic increase in  $\text{HO}^\bullet$  generation in a short time. However, the reaction between  $\text{HO}^\bullet$  and  $\text{Fe(II)}$  can scavenge  $\text{HO}^\bullet$  leading to a low  $\text{HO}^\bullet$  yield (Eq. 6), and the rapid generation of  $\text{HO}^\bullet$  can also favor radical-radical reactions over radical-organic reactions, therefore limiting the detection of the generated radicals [11]. Fig. 2d shows when the molar ratios of  $\text{CaO}_2/\text{Fe(II)}$  were 1/2 and 1/4, the consumed  $\text{Fe(II)}$  was 60% and 30%, respectively. The similar consumption of  $\text{Fe(II)}$  and  $\text{H}_2\text{O}_2$  led to a comparable  $\text{HO}^\bullet$  generation, and as a result, the actual generation of  $\text{HO}^\bullet$  was similar in these two  $\text{CaO}_2/\text{Fe(II)}$  molar ratio conditions.

The above results showed that too much  $\text{CaO}_2$  or  $\text{Fe(II)}$  does not benefit  $\text{HO}^\bullet$  generation, and that the  $\text{HO}^\bullet$  yield depends on an optimal molar ratio of  $\text{CaO}_2/\text{Fe(II)}$ , which is consistent with previous reports [3–7]. However, our results further indicated that the  $\text{HO}^\bullet$  generation efficiency was more sensitive to the changes of  $\text{CaO}_2$  compared to that of  $\text{Fe(II)}$ . Fixing  $\text{Fe(II)}$  at 1 mM, the  $\text{HO}^\bullet$  generation efficiency decreased from 34% to 6% when the initial  $\text{CaO}_2$  dosage increased from 0.5 to 4 mM (Table 2). In contrast, the  $\text{HO}^\bullet$  generation efficiency decreased from 38% to 26% when the initial  $\text{Fe(II)}$  dosage increased from 0.5 to 4 mM when fixing  $\text{CaO}_2$  at 1 mM (Table 2). The results suggest that regulating  $\text{Fe(II)}$  could be

more convenient and practical to improve the performance of the  $\text{CaO}_2/\text{Fe(II)}$  system in terms of  $\text{HO}^\bullet$  generation efficiency.

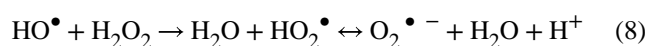
The variation of pH during the experiments was also monitored, and the results showed that the impacts caused by the reagents were different (Table 2). The  $\Delta\text{pH}$  ( $\Delta\text{pH} = \text{final pH} - \text{initial pH}$ ) increased with the increase of  $\text{CaO}_2$  dosage, while slight changes in  $\Delta\text{pH}$  were found when varying  $\text{Fe(II)}$  from 0.5 to 4.0 mM. However, the  $\Delta\text{pH}$  range was limited ( $\Delta\text{pH} < 1$ ) in most experiments except for  $\text{CaO}_2/\text{Fe(II)}$  molar ratio of 4/1. The solution pH increased with increasing  $\text{CaO}_2$  dosage, with pH greater than 5.0 when 4.0 mM  $\text{CaO}_2$  was applied. This increase in pH suppressed the Fenton reaction. Hence, it is necessary to further clarify the effect of pH on  $\text{HO}^\bullet$  generation.

**3.1.2 Effect of solution pH on  $\text{HO}^\bullet$  formation**—Fig. 3a illustrates the effect of the initial solution pH (without buffer) on  $\text{HO}^\bullet$  generation. With the pH elevation from 3 to 10, the detected  $\text{HO}^\bullet$  decreased from 0.36 to 0.018 mM.  $\text{HO}^\bullet$  yield significantly declined with the increase of solution pH (Fig. 3b). The results suggest that an acidic environment is more favorable to  $\text{HO}^\bullet$  generation in the  $\text{CaO}_2/\text{Fe(II)}$  system, and this trend is consistent with the general observation in Fenton reactions in which the optimum solution pH value for Fenton oxidation process is approximately 3.

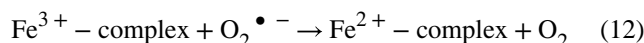
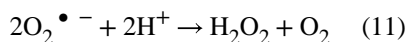
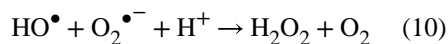
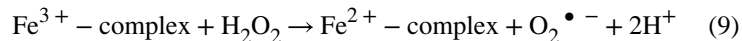
It is obvious that the majority of  $\text{Fe(II)}$  was consumed in a short time (Fig. 3c), and p-HBA generation was rapid subsequent to the  $\text{HO}^\bullet$  surge. When the initial  $\text{pH} > 4$ ,  $\text{Fe(II)}$  dropped sharply (Fig. 3c) and the shortage of  $\text{Fe(II)}$  can limit  $\text{HO}^\bullet$  generation. Fig. 3d shows that for  $\text{pH} \leq 4$  the monitored  $\text{H}_2\text{O}_2$  increased sharply, after which the residual  $\text{H}_2\text{O}_2$  declined steadily as a single-peak curve. However, different  $\text{H}_2\text{O}_2$  patterns were observed when the  $\text{pH} > 4$ . Less  $\text{H}_2\text{O}_2$  was detected at the very beginning of the reaction when  $\text{pH} = 5.5 \sim 10$  (Fig. 3d). Northup and Cassidy [1] reported that the increase of solution pH would lower the dissolution rate of  $\text{CaO}_2$  and  $\text{H}_2\text{O}_2$  yields; meanwhile, the rapid consumption of  $\text{Fe(II)}$  in the beginning exacerbated the exhaustion of  $\text{H}_2\text{O}_2$  from  $\text{CaO}_2$ . Therefore, although  $\text{HO}^\bullet$  rose sharply,  $\text{H}_2\text{O}_2$  was not detected in the beginning when  $\text{pH} > 4$ . The monitored  $\text{H}_2\text{O}_2$  then increased markedly and presented moderate downward trends in the following period when  $\text{pH} > 4$ , and the residual  $\text{H}_2\text{O}_2$  was obviously higher because of the insignificant  $\text{H}_2\text{O}_2$  decomposition as a result of  $\text{Fe(II)}$  shortage. This behavior differs greatly from the results when  $\text{pH} < 4$  (Fig. 3d). In addition, the generation of  $\text{HO}^\bullet$  in the  $\text{CaO}_2$  based system at neutral and alkaline pH conditions was deduced based on contaminant degradation behavior in previous studies [3,5–7]. The detected p-HBA in this study provides direct evidence that  $\text{HO}^\bullet$  is generated in the  $\text{CaO}_2/\text{Fe(II)}$  system at neutral and alkaline pH conditions (Fig. 3b).

### 3.2 $\text{O}_2^{\bullet-}$ generation in the $\text{CaO}_2/\text{Fe(II)}$ Fenton system

Besides  $\text{HO}^\bullet$ ,  $\text{O}_2^{\bullet-}$  is another possible ROS involved in the  $\text{CaO}_2$  based system.  $\text{O}_2^{\bullet-}$  propagation and termination in Fenton reactions are presented by Eqs. 8 ~ 12.







Based on Eq. 3, NBT was used to capture  $\text{O}_2^{\bullet-}$  produced in the  $\text{CaO}_2$  based system, and the preliminary study confirmed  $\text{O}_2^{\bullet-}$  was produced in the  $\text{CaO}_2/\text{Fe(II)}$  Fenton system (Supplementary Material, Text S3, Fig. S4).

The effects of  $\text{CaO}_2$  and  $\text{Fe(II)}$  dosage on  $\text{O}_2^{\bullet-}$  production were investigated. The results indicate that  $\text{O}_2^{\bullet-}$  production increased with the  $\text{CaO}_2$  dosage, but  $\text{O}_2^{\bullet-}$  variations were not strictly proportional to  $\text{CaO}_2$  dosage (Supplementary Material, Text S4, Fig. S5a). Fig. S6 suggests that  $\text{O}_2^{\bullet-}$  can be produced through different pathways. For the  $\text{CaO}_2$  based Fenton system,  $\text{O}_2^{\bullet-}$  can be produced by the Fenton pathway through various reactions as a result of  $\text{H}_2\text{O}_2$  decomposition (Eqs. 8 ~ 12). The results in Fig. S6 also indicate that  $\text{O}_2^{\bullet-}$  can be generated via a non-Fenton pathway wherein  $\text{CaO}_2$  reacts with water (Eqs. 13, 8 & 9) [8,42,43]. Too much  $\text{CaO}_2$  can depress the Fenton-pathway based  $\text{O}_2^{\bullet-}$  generation but has less influence on the non-Fenton pathway  $\text{O}_2^{\bullet-}$  generation (Supplementary Material, Text S4) [8].

In contrast, too much  $\text{Fe(II)}$  can produce more  $\text{Fe(III)}$ , and the increase of  $\text{Fe(III)}$  can increase  $\text{O}_2^{\bullet-}$  scavenging, leading to low  $\text{O}_2^{\bullet-}$  yield (Fig. S5b). Moreover, the decline of  $\text{HO}^\bullet$  also constrained  $\text{O}_2^{\bullet-}$  generation pathways. The influence of initial solution pH (from 3 to 10) on  $\text{O}_2^{\bullet-}$  generation was also studied. The lowest  $\text{O}_2^{\bullet-}$  peak was observed at  $\text{pH} = 3$  when the highest  $\text{HO}^\bullet$  yield was observed. The absorbance was even slightly enhanced when increasing pH to 10 (Supplementary Material, Text S5, Fig. S7), suggesting that the alkaline solution pH could be efficient in encouraging  $\text{O}_2^{\bullet-}$  generation.



### 3.3 ROS generation mechanism in the $\text{CaO}_2/\text{Fe(II)}$ system

Based on the experimental results, the proposed mechanism of ROSs generation in the  $\text{CaO}_2/\text{Fe(II)}$  system is displayed in Fig. 4.

The  $\text{CaO}_2$  dissolution process in water is slow, but the dissolved  $\text{CaO}_2$  can rapidly produce  $\text{H}_2\text{O}_2$  in aqueous solution [43]. The addition of  $\text{Fe(II)}$  initiates the Fenton reaction.  $\text{Fe(II)}$  reacts with the produced  $\text{H}_2\text{O}_2$  to generate  $\text{HO}^\bullet$  and  $\text{O}_2^{\bullet-}$ , which are confirmed by the p-HBA generation and NBT tests, respectively. The produced  $\text{H}_2\text{O}_2$  can possibly obtain an electron leading to the non-Fenton pathway which can generate  $\text{HO}^\bullet$  and  $\text{O}_2^{\bullet-}$  [5,8]. Compared with the non-Fenton pathway, the Fenton pathway is the major reactive species source, and  $\text{HO}^\bullet$  is the primary radical in the  $\text{CaO}_2/\text{Fe(II)}$  system. The molar ratio of  $\text{CaO}_2/\text{Fe(II)}$  can change the performance of the Fenton reactions, resulting in different radicals distribution. The solution pH can affect  $\text{CaO}_2$  dissolution performance, thereby altering  $\text{H}_2\text{O}_2$  release and lead to different radical yields.

### 3.4 New strategy for the enhancement of $\text{HO}^\bullet$ formation

Due to its reactive properties of non-selectivity and high efficiency with most organic contaminants,  $\text{HO}^\bullet$  is the key reactive species in the  $\text{CaO}_2/\text{Fe(II)}$  system. Based on the prior analysis, pH and the molar ratio of  $\text{CaO}_2/\text{Fe(II)}$  can influence the  $\text{HO}^\bullet$  generation efficiency. However, pH adjustment is difficult to implement for subsurface systems and requires additional acid chemicals. Thus, regulating the molar ratio of  $\text{CaO}_2/\text{Fe(II)}$  is the easier, more effective way to optimize  $\text{HO}^\bullet$  generation efficiency. Since rapid  $\text{HO}^\bullet$  generation can constrain  $\text{HO}^\bullet$  efficiency, it is necessary to study if moderate reaction benefits more  $\text{HO}^\bullet$  generation.  $\text{CaO}_2$  is stable and can release  $\text{H}_2\text{O}_2$  for a relatively long time [1,43], and the dosage of  $\text{Fe(II)}$  has the potential to affect the  $\text{HO}^\bullet$  yield. Hence,  $\text{Fe(II)}$  could be the more suitable factor regulating  $\text{HO}^\bullet$  generation (Supplementary Material, Text S6). Changing  $\text{Fe(II)}$  dosing method from the single dose to sequential addition might be an option to optimize  $\text{HO}^\bullet$  generation, which can constrain the competition reactions.

After two-step additions of  $\text{Fe(II)}$  (0.5 mM for each time), the final molar ratio of  $\text{CaO}_2/\text{Fe(II)}$  reached 1/1, and the overall  $\text{HO}^\bullet$  was 0.41 mM (Fig. 5a). It is noted that  $\text{HO}^\bullet$  generation was significantly accelerated after the second dosing of  $\text{Fe(II)}$ , and the two-step additions of  $\text{Fe(II)}$  also improved  $\text{HO}^\bullet$  generation by 14% in comparison to the same final concentration of  $\text{CaO}_2/\text{Fe(II)}$  (single step addition of  $\text{Fe(II)}$ ). This test demonstrates that is feasible to control  $\text{HO}^\bullet$  generation by varying the  $\text{Fe(II)}$  dosing method.

An additional experiment test was conducted to further test this hypothesis, in which  $\text{Fe(II)}$  solution was transferred successively within 120 min by a persist pump to the reactor containing a  $\text{CaO}_2/\text{BA}$  molar ratio of 1/10 and reaching the final molar ratio of  $\text{CaO}_2/\text{Fe(II)} = 1/1$ . With the successive addition of  $\text{Fe(II)}$ ,  $\text{HO}^\bullet$  was steadily generated in the  $\text{CaO}_2/\text{Fe(II)}$  system, and in this situation  $\text{HO}^\bullet$  generation presented a curve which was similar to the change of  $\text{Fe(II)}$  amount but different from other  $\text{HO}^\bullet$  generation curves (Fig. 5a and 5b). This result showed that  $\text{HO}^\bullet$  generation can be manipulated by successively dosing  $\text{Fe(II)}$ , and the final  $\text{HO}^\bullet$  was increased to 0.49 mM, representing an increase of 37% in  $\text{HO}^\bullet$  generation.

The changes of Fe(II) and H<sub>2</sub>O<sub>2</sub> during the course of sequential addition of Fe(II) are given in Figs. 5b and 5c. In the two-step additions of Fe(II) test, the value of Fe(II) exhibited a stepwise increase, while H<sub>2</sub>O<sub>2</sub> presented a sharp drop when the other half Fe(II) was added to the reactor. The trends in the successive addition of Fe(II) test were completely different. With a continuous increment of Fe(II), the available Fe(II) rose moderately, and H<sub>2</sub>O<sub>2</sub> dramatically increased and then steadily dropped as a single-peak curve. The lower Fe(II) concentration, the same final H<sub>2</sub>O<sub>2</sub> concentration as well as the higher HO• generation indicated that the reaction was successfully tuned by gradually dosing Fe(II). The successively dosing Fe(II) contributed to a slow and steady production of HO•, and played an important role in the CaO<sub>2</sub>/Fe(II) system. It was obvious that successively providing Fe(II) could decrease HO• generation rate, and the generated HO• would prefer to react with BA [11]. In addition, the scavenging of HO• by Fe(II) and HO• self-reaction were also limited, hence resulted in a higher HO• generation [11,43]. Therefore, combining the successive dosing of Fe(II) with the application of CaO<sub>2</sub> can be a more efficient and convenient strategy to treat contamination.

This strategy has implications for using *in situ* chemical oxidation employing CaO<sub>2</sub> to treat contaminated groundwater. A possible application scheme and model is shown in Fig. 6. In the injection and transport steps, after dosing the proper conditioning reagents, CaO<sub>2</sub> slurry is first injected into the contaminated groundwater, spreading into the contamination zone. Then the treatment process can be regulated by injecting Fe(II) solution. When Fe(II) is periodically pumped into the zone, Fe(II) starts the Fenton reaction, and can also decrease the solution pH and accelerate H<sub>2</sub>O<sub>2</sub> generation, which benefits the Fenton process. When the contaminant is completely oxidized, the reaction can be halted by stopping injection of Fe(II) solution. However, the groundwater flow and background solution matrix are different from the experimental conditions, which may affect CaO<sub>2</sub> migration, H<sub>2</sub>O<sub>2</sub> generation, and the Fenton reaction efficiency (Supplementary Material, Fig. S8). And the influence of CaO<sub>2</sub> based Fenton system on the groundwater ecosystem is another concern, which requires more investigation in the future.

#### 4. Conclusion

The generation of ROSs in the CaO<sub>2</sub>/Fe(II) system was investigated. BA and NBT were applied as probe compounds to capture the generated HO• and O<sub>2</sub>•<sup>-</sup>, respectively. For HO•, the CaO<sub>2</sub> based Fenton reaction was the main source, and the dosage of CaO<sub>2</sub> and Fe(II) greatly affected HO• generation, suggesting an optimal molar ratio of CaO<sub>2</sub>/Fe(II) was required for optimization of HO• yield. The CaO<sub>2</sub>/Fe(II) system favored the acidic environment in terms of HO• generation. For CaO<sub>2</sub> based Fenton system, O<sub>2</sub>•<sup>-</sup> can be produced through various reactions initiated by Fe(II) and H<sub>2</sub>O<sub>2</sub> forming Fenton pathway, and can also be directly generated when CaO<sub>2</sub> reacts with water developing a non-Fenton pathway. The O<sub>2</sub>•<sup>-</sup> generation was more sensitive to the CaO<sub>2</sub> dosage. The influence of solution pH on O<sub>2</sub>•<sup>-</sup> generation was different from that on HO•. The sequential dosing of Fe(II) can be an efficient strategy to generate higher HO• in the CaO<sub>2</sub>/Fe(II) system, showing a potential application of this technique for groundwater remediation.

## Supplementary Material

Refer to Web version on PubMed Central for supplementary material.

## Acknowledgement

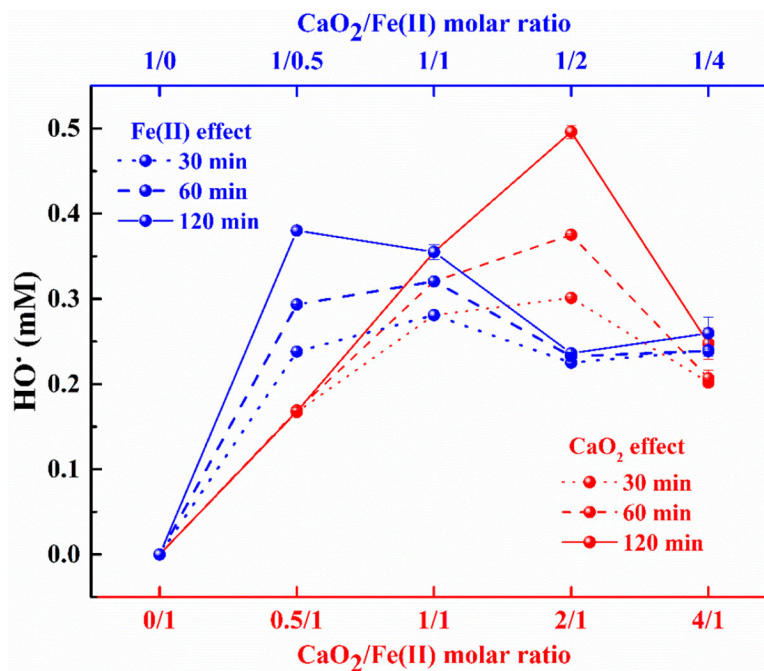
This study was financially supported by the grant from the National Natural Science Foundation of China (41373094), Natural Science Foundation of Shanghai, China (16ZR1407200). The contributions of Mark Brusseau were supported by the NIEHS Superfund Research Program (PS 42 ES04940).

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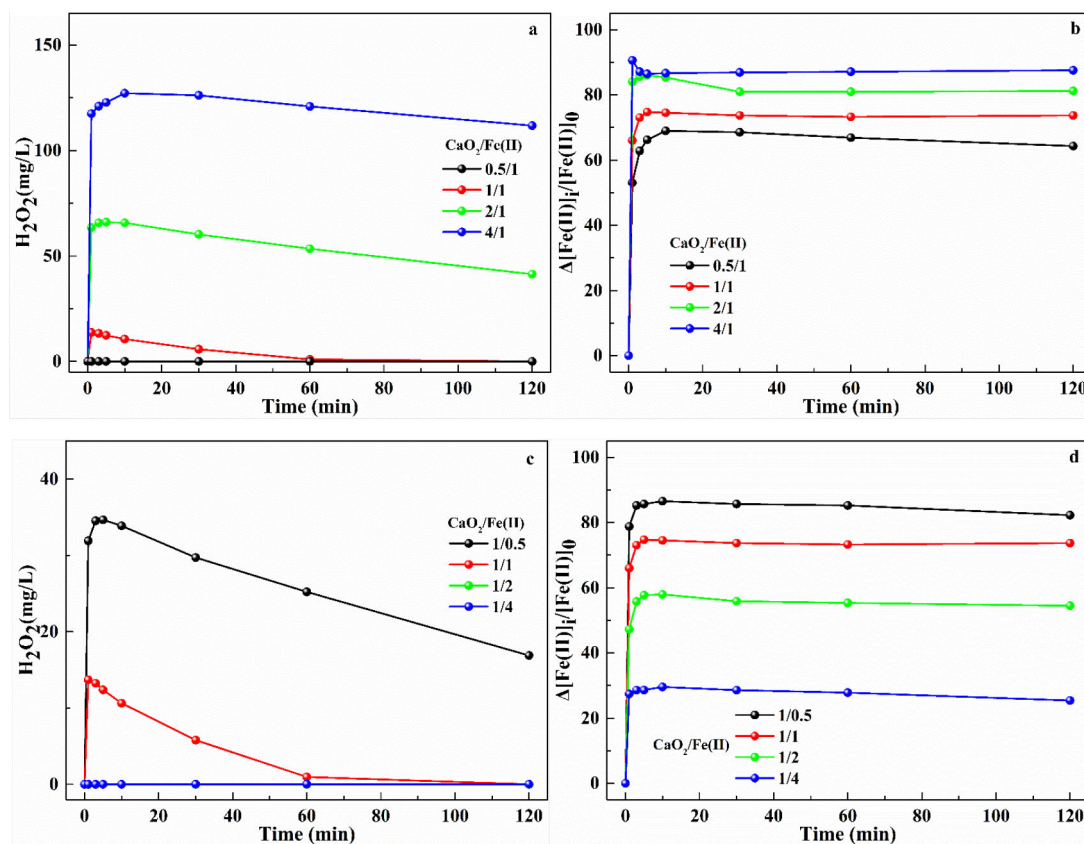
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**Fig. 1.**

(a) The influences of CaO<sub>2</sub> and Fe(II) dosages on HO• generation. (The molar ratios of CaO<sub>2</sub>/Fe(II) = 1/0, 1/0.5, 1/1, 1/2, 1/4, 0/1, 0.5/1, 1/1, 2/1, 4/1, [CaO<sub>2</sub>]<sub>0</sub> or [Fe(II)]<sub>0</sub> was fixed as 1 mM, [BA]<sub>0</sub> = 10 mM. [HO•] = 5.87 × [p-HBA]), (b) HPLC chromatograms of the p-HBA and BA. ([CaO<sub>2</sub>]<sub>0</sub> = [Fe(II)]<sub>0</sub> = 1.0 mM, [BA]<sub>0</sub> = 10 mM).

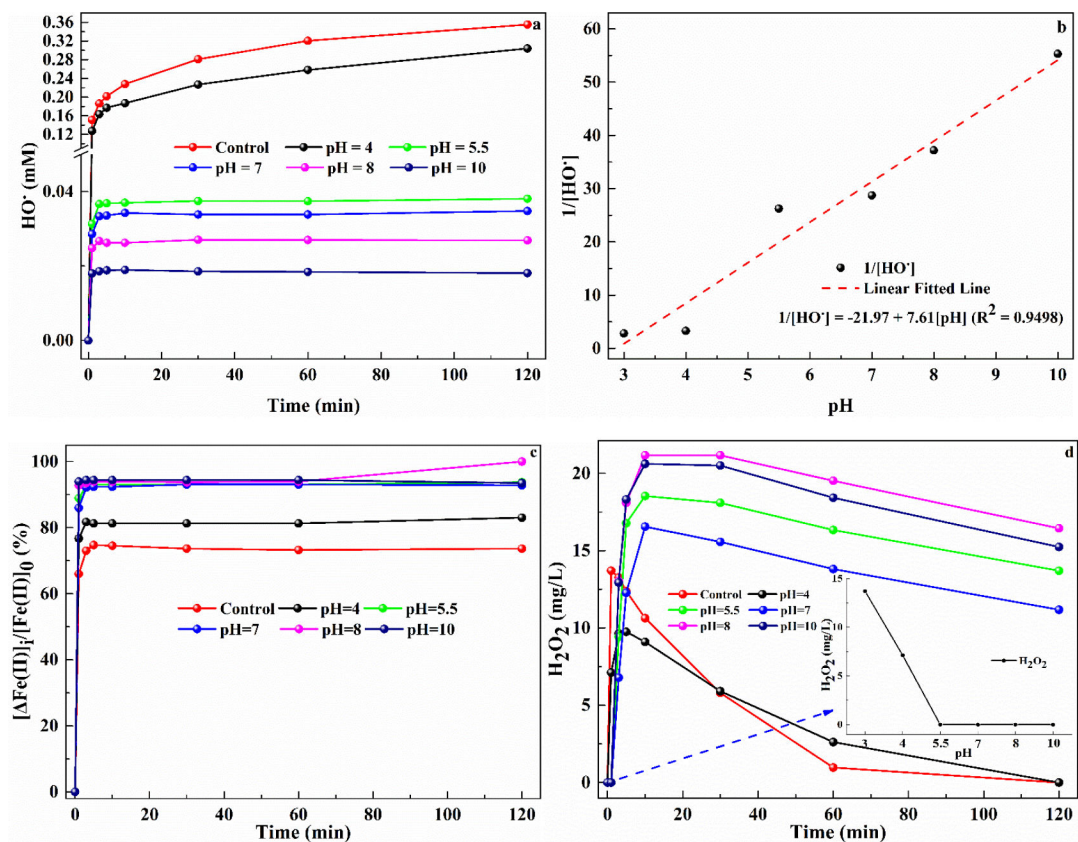




**Fig. 2.**

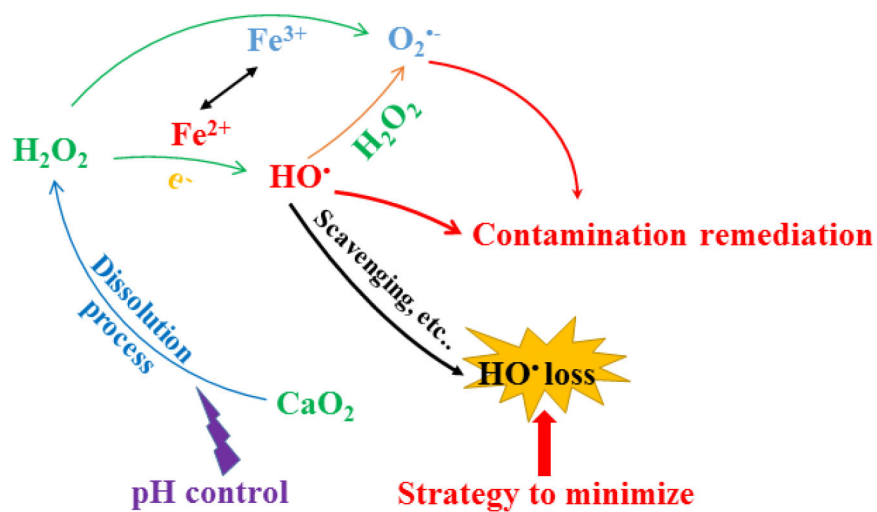
The influences of  $\text{CaO}_2$  on variations of (a)  $\text{H}_2\text{O}_2$  and (b)  $\text{Fe(II)}$  (The molar ratios of  $\text{CaO}_2/\text{Fe(II)} = 1/0.5, 1/1, 1/2, 1/4, 0.5/1, 1/1, 2/1, 4/1$ ,  $[\text{Fe(II)}]_0 = 1.0 \text{ mM}$ ,  $[\text{BA}]_0 = 10 \text{ mM}$ ); and the influences of  $\text{Fe(II)}$  on variations of (c)  $\text{H}_2\text{O}_2$  and (d)  $\text{Fe(II)}$  (The molar ratios of  $\text{CaO}_2/\text{Fe(II)} = 1/0.5, 1/1, 1/2, 1/4, 0.5/1, 1/1, 2/1, 4/1$ ,  $[\text{CaO}_2]_0 = 1.0 \text{ mM}$ ,  $[\text{BA}]_0 = 10 \text{ mM}$ ).



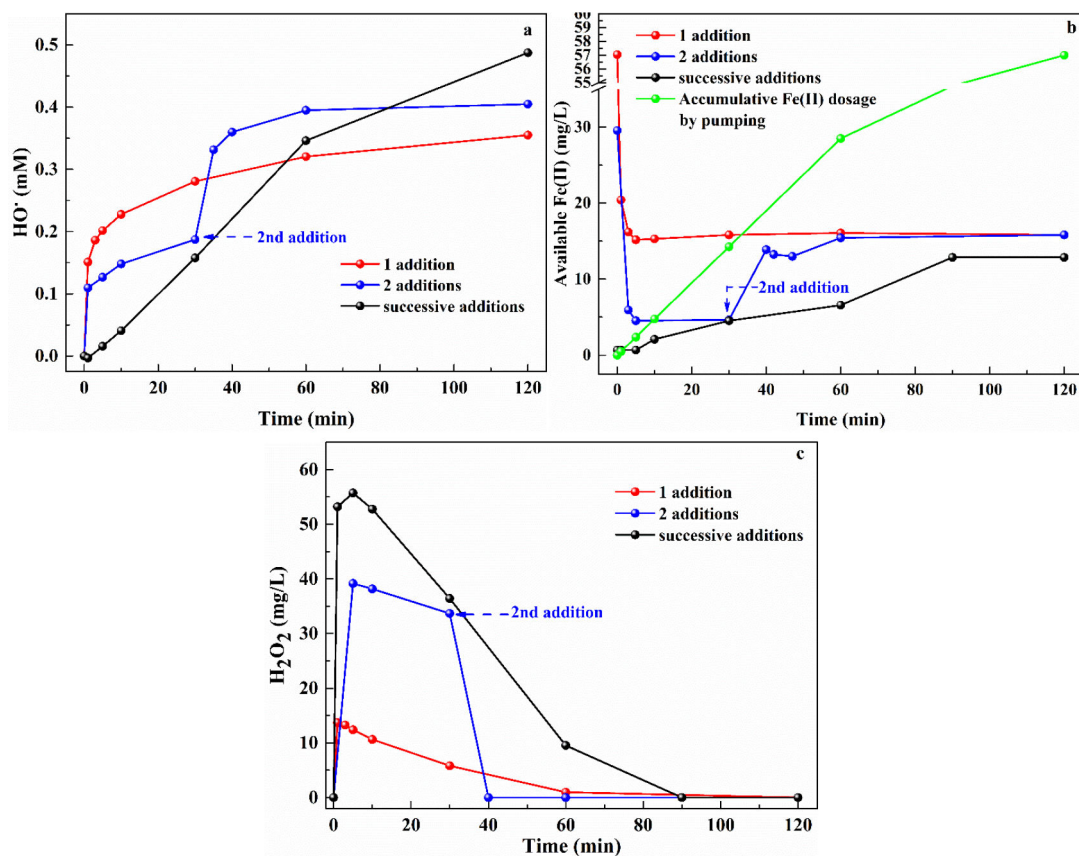


**Fig. 3.**

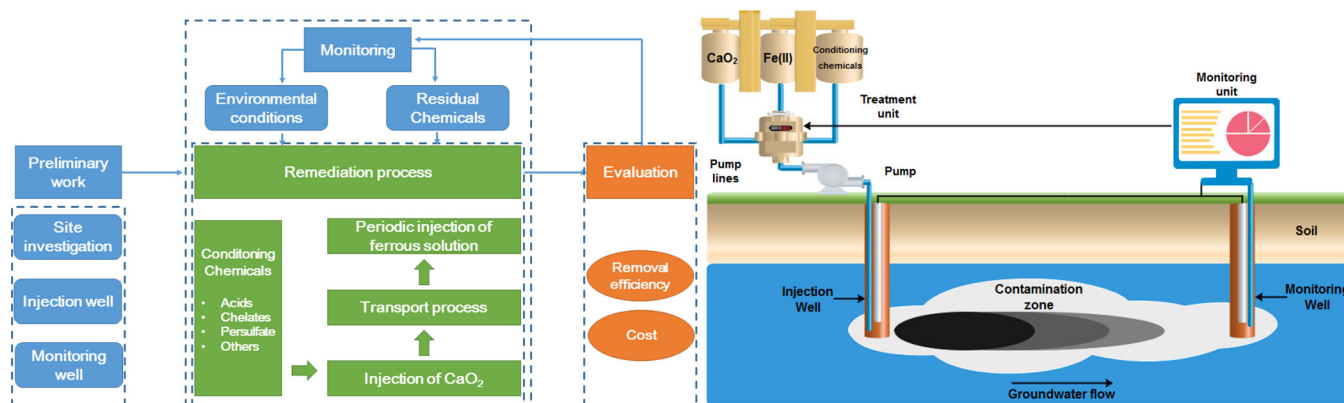
(a) The influences of pH on HO<sup>•</sup> generation, (b) The relationship between pH and HO<sup>•</sup>; and the influences of pH on changes of (c) Fe(II) and (d) H<sub>2</sub>O<sub>2</sub>: insert graph: the detected H<sub>2</sub>O<sub>2</sub> concentration at 1 min. ([CaO<sub>2</sub>]<sub>0</sub> = [Fe(II)]<sub>0</sub> = 1.0 mM, [BA]<sub>0</sub> = 10 mM, [HO<sup>•</sup>] = 5.87 × [p-HBA], the pH of control experiment was 3).



**Fig. 4.**  
The reactive species in the  $\text{CaO}_2/\text{Fe(II)}$  system.

**Fig. 5.**

The influences of sequential addition of Fe(II) on (a) HO• generation, and (b) variations of available Fe(II) and (c) variations of available H<sub>2</sub>O<sub>2</sub>. ([CaO<sub>2</sub>]<sub>0</sub> = [Fe(II)]<sub>0</sub> = 1.0 mM [BA]<sub>0</sub> = 10 mM, [HO•] = 5.87 × [p-HBA]).



**Fig. 6.** Illustration for the possible application of the  $\text{CaO}_2/\text{Fe(II)}$  technique.

**Table 1**

The rate constants for the reactions between probe compounds and  $\text{HO}^\bullet$ , and the features of the probe compounds in  $\text{O}_2^{\bullet-}$  determination

Probe compound	Reaction	k	Ref.
Coumarin	$\text{C}_9\text{H}_6\text{O}_2 + 2 \text{HO}^\bullet \rightarrow \text{C}_9\text{H}_6\text{O}_3 + \text{H}_2\text{O}$	$6.2 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	[18]
Salicylic acid	$\text{C}_7\text{H}_6\text{O}_2 + 2 \text{HO}^\bullet \rightarrow \text{C}_7\text{H}_6\text{O}_3$	$5 \times 10^9 \sim 5 \times 10^{10} \text{ M}^{-1} \text{ s}^{-1}$	[19]
$\text{HO}^\bullet$ Benzoic acid	$\text{C}_6\text{H}_5\text{CO}_2\text{H} + \text{HO}^\bullet \rightarrow \text{HOC}_6\text{H}_5\text{CO}_2\text{H}$	$5.9 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	
1-Propanol	$(\text{CH}_3)_2\text{CHOH} + \text{HO}^\bullet \rightarrow \text{C}_3\text{H}_6\text{O}$	$1.9 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$	[23]
$\text{Fe}^{2+}$	$\text{Fe}^{2+} + \text{HO}^\bullet \rightarrow \text{Fe}^{3+} + \text{OH}^-$	$4.3 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$	

Probe compound	Features	Ref.
Luminol	Non-selective probes; $\text{O}_2^{\bullet-}$ determined by generated chemiluminescence; $\text{pK}_{\text{a}1} = 6.3$ , $\text{pK}_{\text{a}2} = 15.21$	[24,25]
MCLA	Sensitive and wide applicable pH range; $\text{O}_2^{\bullet-}$ determined by generated chemiluminescence; $\text{pK}_{\text{a}} = 7.75$	[26]
$\text{O}_2^{\bullet-}$ NBT	Not influenced by $\text{H}_2\text{O}_2$ and $\text{HO}^\bullet$ ; $\text{O}_2^{\bullet-}$ determined by the direct absorbance of NBT solution or the indirect absorbance of NBT-formazan; $k(\text{O}_2^{\bullet-}) = 5.9 \times 10^4 \text{ M}^{-1} \text{ s}^{-1}$	[27–29]
XTT	Selective and good water solubility; $\text{O}_2^{\bullet-}$ determined by the absorbance of XTT solution; $k(\text{O}_2^{\bullet-}) = 8.59 \times 10^4 \text{ M}^{-1} \text{ s}^{-1}$	[30]

**Table 2**

HO<sup>●</sup> initial formation rates, pH variations and pH influence on the HO<sup>●</sup> yield in the CaO<sub>2</sub>/Fe(II) system

	CaO <sub>2</sub> /Fe(II) <sup>a</sup>	k <sup>b</sup> (M <sup>-1</sup> s <sup>-1</sup> )	pH variation <sup>c</sup>	HO <sup>●</sup> yield <sup>d</sup> (%)
Influence of CaO <sub>2</sub>	0.5/1	1.98 × 10 <sup>-6</sup>	3.01/3.06; 0.05	33.72
	2/1	2.77 × 10 <sup>-6</sup>	3.05/3.89; 0.84	24.90
	4/1	2.55 × 10 <sup>-6</sup>	3.08/5.21; 2.13	6.22
	1/1	2.51 × 10 <sup>-6</sup>	3.07/3.38; 0.31	35.65
Influence of Fe(II)	1/0.5	2.08 × 10 <sup>-6</sup>	3.05/3.50; 0.45	38.17
	1/2	2.86 × 10 <sup>-6</sup>	3.07/3.14; 0.07	23.70
	1/4	2.38 × 10 <sup>-6</sup>	3.09/3.11; 0.02	26.08

	pH	HO <sup>●</sup> yield <sup>d</sup> (%)
Influence of pH	3	35.65
	4	30.41
	5.5	3.81
	7	3.48
	8	2.69
	10	1.81

<sup>a</sup>: Molar ratio;

<sup>b</sup>: Initial rate of HO<sup>●</sup> formation;

<sup>c</sup>: Initial pH/Final pH; pH = final pH- initial pH;

<sup>d</sup>: Based on the theoretical calculation: 0.47 g H<sub>2</sub>O<sub>2</sub>/g CaO<sub>2</sub>, and all the released H<sub>2</sub>O<sub>2</sub> participated in Fenton reaction.